# Geomagnetic field intensity during the last 5 Myr: LTD-DHT Shaw palaeointensities from volcanic rocks of the Society Islands, French Polynesia

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#### SUMMARY

On the basis of the Thellier palaeointensities reported so far it has been thought that the timeaveraged virtual dipole moment (VDM) and virtual axial dipole moment (VADM) for the last few million years are almost the same as the present geomagnetic dipole moment ( $\sim 8 \times$  $10^{22}$  A m<sup>2</sup>). This estimate has been called into question, however, because recent studies have revealed that the Thellier method occasionally overestimates palaeointensities by as much as twice the true values. In contrast, a recently developed palaeointensity technique, namely the double heating technique of the Shaw method combined with low-temperature demagnetization (the LTD-DHT Shaw method), can yield expected field intensities from samples which give unreliable palaeointensities using the Thellier method. Therefore, we have measured absolute palaeointensities from 0.5–4.6 Ma volcanic rocks from the Society Islands, French Polynesia, mainly using the LTD-DHT Shaw method. As a result, 195 out of 361 samples passed the selection criteria, some of which are compared with additional results obtained with Coe's version of the Thellier method. In the Thellier experiments, 18 out of 40 samples passed the criteria, giving palaeointensities both consistent and inconsistent with the LTD-DHT Shaw results. These samples are characterized mostly by two-segmented Arai diagrams. If we take the LTD-DHT Shaw palaeointensities, 24 reliable site means are available and give a mean VADM of  $(3.64 \pm 2.10) \times 10^{22}$  A m<sup>2</sup>. This is nearly half of the mean of the 0–5 Ma Thellier data selected from the latest palaeointensity database [ $(7.46 \pm 3.10) \times 10^{22}$  A m<sup>2</sup>, N = 458] as well as the present dipole moment. The LTD-DHT Shaw palaeointensities newly determined in this study suggest that the present-day field is so strong that it may not be typical of the past geomagnetic field.

**Key words:** French Polynesia, LTD-DHT Shaw method, Palaeointensity, Society Islands, Thellier method.

## **1 INTRODUCTION**

The main geomagnetic field has its origin in the Earth's outer core. Since a dipole component is dominant in the field, information about temporal changes, the average and the deviation of the moment is essential for understanding the evolution of the Earth's deep interior. If we can obtain these values, the long-term evolution of the outer core can be evaluated as well as its current activity. For the period of the last 5 Myr McFadden & McElhinny (1982) estimated a time-averaged virtual dipole moment (VDM) of  $(8.67 \pm 3.63) \times 10^{22}$  A m<sup>2</sup>, which is almost the same as the present geomagnetic dipole moment (~ 8 × 10<sup>22</sup> A m<sup>2</sup>). This conclusion was not greatly changed in a later analysis of a mean VDM of  $(7.84 \pm 3.80) \times 10^{22}$  A m<sup>2</sup> for the last 10 Myr by Tanaka *et al.* (1995b) using an updated database (Tanaka & Kono 1994).

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However, that database involved a number of palaeointensities obtained by methods other than the Thellier method (Thellier & Thellier 1959). Since many palaeomagnetists regard the Thellier method as the only reliable one (e.g. Selkin & Tauxe 2000; Goguitchaichvili *et al.* 2004), Juarez & Tauxe (2000) questioned the quality of the database. They carefully examined a further updated database (Perrin *et al.* 1998) applying more stringent selection criteria and rejecting data other than the Thellier palaeointensities. Adding their new Thellier palaeointensities from submarine basaltic glasses, they determined the time-averaged virtual axial dipole moment (VADM) for 0.3-5 Ma to be  $(5.49 \pm 2.36) \times 10^{22}$  A m<sup>2</sup>. This is lower than the both previous values (McFadden & McElhinny 1982; Tanaka *et al.* 1995b) and the present dipole moment.

Since the work of Juarez & Tauxe (2000), a number of researchers have been making efforts to increase the number of absolute palaeointensity data. The latest palaeointensity database (Perrin & Schnepp 2004) contains 3128 items from 215 references. The number of data has almost tripled compared with the 1995 database (1123 items from 83 original papers in Tanaka et al. 1995b). Contrary to the conclusion by Juarez & Tauxe (2000), the majority of new measurements by the Thellier method showed high palaeointensities. For example, Laj et al. (2000) reported 89 Thellier results from 2.1-3.9 Ma lavas in Oahu, Hawaii, obtaining an average VADM of  $(7.0 \pm 2.3) \times 10^{22}$  A m<sup>2</sup>. Bogue (2001) gave an average VDM of  $(9.38 \pm 2.43) \times 10^{22}$  A m<sup>2</sup> from 25 site mean palaeointensities of 4 Ma lava flows from Kauai, Hawaii. Alva-Valdivia et al. (2001) reported palaeointensities from four lava flows erupted between 0.8 and 2.2 Ma in Mexico and the resultant VDMs ranged from 6.4 to  $9.1 \times 10^{22}$  A m<sup>2</sup>. Recent statistical analyses by Heller *et al.* (2002) on their own Thellier palaeointensity database revealed that the average VDM for the last 5 Myr resulted in  $\sim 8 \times 10^{22}$  A m<sup>2</sup> (Fig. 6 of Heller et al. 2002). A comprehensive review by Valet (2003) also concluded the mean VADM for the past 4 Myr volcanic Thellier-Thellier records was  $(7 \pm 3.6) \times 10^{22}$  A m<sup>2</sup>. These conclusions have been supported by Leonhardt et al. (2003). They obtained 42 new Thellier data from 1.8-3.3 Ma Brazilian volcanic rocks that resulted in VADM of  $(7.5 \pm 2.6) \times 10^{22}$  A m<sup>2</sup> (N = 10). The Thellier method still seems to yield high palaeointensities.

It is possible to say that these high palaeointensities are misreadings of the ancient geomagnetic field, because recent studies have pointed out that the Thellier method occasionally fails in accurate determination of palaeointensity from historical lavas. Biggin & Thomas (2003a) demonstrated that the usual selection criteria of the Thellier method (e.g.  $N \ge 4, q \ge 5$ , where N is the number of data points and q the quality factor of Coe et al. 1978) could not discriminate incorrect palaeointensities. Yamamoto et al. (2003) showed that the Kilauea 1960 lava in Hawaii yielded systematically higher Thellier palaeointensities (up to twice the expected value). Such bad results have also been reported in conventional Thellier experiments (Tanaka & Kono 1991) and in modern microwave Thellier experiments (Hill & Shaw 2000). In a study of the Kilauea 1970 lava (Oishi et al. 2005), two out of seven successful results using the Thellier method showed 46 and 55 per cent higher field intensities than the expected. Anomalous palaeointensities have not been restricted to the Hawaiian lavas. Calvo et al. (2002) obtained 25 per cent larger mean intensities from 1910 and 1928 Mount Etna lavas, Italy. From the Oshima 1986 lava in Japan, Mochizuki et al. (2004) observed palaeointensities exceeding the expected value by up to about 30 per cent. Although the exact value of the expected intensity is unknown, Böhnel et al. (2003) performed both conventional Thellier and microwave Thellier experiments on the AD 330 Xitle lava samples from Mexico, resulting in high palaeointensities up to  $\sim$ 175 and  $\sim$ 155 per cent of the contemporaneous global mean of Yang et al. (2000), respectively.

Samples with an intermediate degree of deuteric oxidization have generally been considered to be very suitable for palaeointensity measurements because of their good thermal stability. However, Yamamoto *et al.* (2003), Mochizuki *et al.* (2004) and Oishi *et al.* (2005) showed that samples with an intermediate degree of high-temperature oxidation of titanomagnetites in particular would yield high palaeointensities by the Thellier method. On the other hand, the double heating technique (DHT) of the Shaw method combined with low-temperature demagnetization (LTD) (LTD-DHT Shaw method; Tsunakawa *et al.* 1997; Yamamoto *et al.* 2003) could give correct answers for samples with various degrees of oxidation. By this method, Yamamoto *et al.* (2003), Mochizuki *et al.* (2004) and Oishi *et al.* (2005) obtained averaged palaeointensities of  $35.7 \pm 3.3 \ \mu\text{T}$  (N = 7),  $46.4 \pm 4.7 \ \mu\text{T}$ (N = 6) and  $38.2 \pm 2.8 \ \mu\text{T}$  (N = 11) from the Kilauea 1960, Oshima 1986 and Kilauea 1970 lavas, respectively. They agreed with the expected values (36.2, 45.5 and  $35.8 \ \mu\text{T}$ ) and were better than the Thellier averages of  $49.0 \pm 9.6 \ \mu\text{T}$  (N = 17),  $51.0 \pm 4.1 \ \mu\text{T}$  (N = 15) and  $43.2 \pm 8.4 \ \mu\text{T}$  (N = 7), respectively.

In this paper we retrieve the geomagnetic dipole moments over the last 5 Myr from volcanic rocks of the Society Islands, French Polynesia, to study the palaeosecular variations (PSV). Most of the palaeointensity measurements were done using the LTD-DHT Shaw method. Although there are several variants of the Thellier-type method, Coe's version of the Thellier method (Coe 1967) was additionally applied to selected samples with good thermal stability aimed at a comparison with traditional palaeointensity databases. With careful experiments and analyses we have obtained reliable palaeointensities. We will discuss the VADM variation for the last 5 Myr, especially its average in comparison with the previous ones.

# 2 SAMPLES AND PREVIOUS PALAEOMAGNETIC STUDIES

The Society Islands consist of 10 volcanic islands and several seamounts. They are of hotspot origin and show a chain-like configuration in a northwest–southeast direction delineating the motion of the Pacific Plate. The present hotspot is located at 18°S, 148°W in the southeastern end of the archipelago (Gripp & Gordon 1990), where several active submarine volcanoes are found. The basaltic volcanism initiated at about 5 Ma (Duncan & McDougall 1976). For these islands, geology, geochemistry and geochronology have been studied by many authors (e.g. Dymond 1975; Duncan & McDougall 1976; Diraison 1991; Duncan *et al.* 1994; Kogiso *et al.* 1997; Blais *et al.* 1997, 2000; Guillou *et al.* 1998; Singer *et al.* 1999). Also about 200 data items on palaeomagnetic direction have been reported (Duncan 1975; Chauvin *et al.* 1990; Roperch & Duncan 1990; White & Duncan 1996).

Regarding palaeointensities, Senanayake et al. (1982) obtained 12 Shaw and 18 Thellier data from the Borabora, Raiatea and Tahiti islands. However, the quality of these data is considered to be insufficient because they used a single heating Shaw method and a Thellier method without a check for partial thermoremanent magnetization (pTRM). Roperch & Duncan (1990) applied the Thellier method to 26 samples from Huahine Island but no satisfactory results were obtained. Only Chauvin et al. (1990) reported successful Thellier results. Twenty-six out of 48 specimens gave 11 distinct site-mean palaeointensities. Three of them  $[37.7 \pm 1.6 \,\mu\text{T} (N = 2)]$ ,  $27.9 \pm 0.8 \ \mu T \ (N = 2)$  and 54.3  $\mu T \ (N = 1)$ ] are from reversely magnetized flows while the others (2.6  $\pm$  0.1  $\mu$ T to 8.1  $\pm$  1.0  $\mu$ T) were from samples with intermediate palaeodirections. The main interest of Chauvin et al. (1990) was in the transitional geomagnetic field, and thus they did not discuss the long-term variation in the geomagnetic dipole moment from the Society volcanic rocks.

Yamamoto *et al.* (2002) recently reported 130 new palaeomagnetic direction data from seven of the Society Islands: Maupiti, Borabora, Tahaa, Raiatea, Huahine, Moorea and Tahiti. Uto *et al.* (submitted) have measured 52 K–Ar ages for those samples. As some sites suffered from secondary magnetizations, both palaeodirections and K–Ar ages were determined for 46 independent sites. These ages are 4.52–4.61 Ma for Maupiti, 3.21–4.01 Ma for Borabora, 2.57–3.24 Ma for Tahaa, 2.45–2.76 Ma for Raiatea, 2.52–3.19 Ma for Huahine, 1.50–1.62 Ma for Moorea and 0.51–1.12 Ma for Tahiti, ranging between 0.51 and 4.61 Ma. The present palaeointensity measurements have been performed mainly on samples from



Figure 1. Map showing the sampling sites.

these sites. The studied samples were collected mostly by a portable engine drill. Orientations were made by a magnetic and/or a sun compass (Yamamoto *et al.* 2002). The site localities are illustrated in Fig. 1.

# **3 ROCK MAGNETIC PROPERTIES**

#### 3.1 Thermomagnetic properties

Thermomagnetic analyses were performed on 53 selected samples using a vibrating sample magnetometer (MicroMag 3900 VSM, Princeton Measurement Corporation). The measurements were done in a helium gas flow with a 500 mT DC field. The resultant  $M_s$ -T curves could be classified into six types: A, B, C, D, E or F (Fig. 2). Except for type E, they are interpreted as magnetization by titanomagnetites with different Ti contents. All the results are listed in Tables 1 and 2. Curie temperatures ( $T_c$ ) were evaluated by the so-called 'intersecting tangents method' (Grommé *et al.* 1969).

Type A curves were observed in 21 samples. They show a single phase of Ti-poor titanomagnetite with good reversibility during the heating and cooling cycle, usually resulting in  $T_c$  higher than 500 °C. Type B curves were recognized in 12 samples and resembled type A, though a minor phase of Ti-rich titanomagnetite with  $T_c$  of 100–400 °C was superimposed. Type C curves were seen in two

samples, showing two components of Ti-poor ( $T_c \sim 560$  °C) and Ti-rich ( $T_c \sim 200$  °C) phases. Type D curves, from five samples, are characterized by a single phase of titanomagnetite with moderate Ti content, the  $T_c$  of which ranges between 140 and 260 °C. They show the some amount of increase in the saturation magnetization ( $M_s$ ) in the cooling stage.

Type E curves are irreversible thermomagnetic curves found in nine samples. They show relatively low- $T_c$  components followed by a small bump of high- $T_c$  ones in the heating curves. Since the high  $T_c$ s ranged from 530 to 580 °C, some amount of titanomaghemite might be initially produced by low-temperature oxidation and transformed into Ti-poor titanomagnetites during the laboratory measurements.

Type F curves were found in four samples. They have the weakest magnetization, and some superparamagnetic behaviour is recognized as a relatively large offset in  $M_s/M_{s0}$ .

#### 3.2 Low-temperature magnetometry

Low-temperature magnetometry was performed on 45 samples with a low-temperature SQUID susceptometer (Quantum Design MPMS-XL5). Saturation isothermal remanent magnetization (SIRM) was imparted to samples under a 2.5 T field at 300 K, and then their remanences were continuously measured in a nearly zero



Figure 2. Six types of thermomagnetic curves (black, heating; grey, cooling). All measurements are performed in a helium gas flow with a DC field of 500 mT.

field by cycling temperatures between 300 and 6 K, sometimes 2 K. For 36 of the samples, sister chip samples were subjected to thermomagnetic analyses as described in the previous subsection. The results are grouped into five types: 26 results for Type a, two results for Type b, 13 results for Type c, two results for Type d and also two results for Type e, as shown in Fig. 3. The categorized groups are listed in Tables 1 and 2.

Type a is characterized by loss and partial recovery of SIRM around 100–120 K, implying a presence of nearly Ti-free titanomagnetite because magnetite shows the isotropic point ( $T_1$ ) around 130 K and the Verwey transition temperature ( $T_v$ ) around 120 K (Dunlop & Özdemir 1997). A similar curve is often observed in marine sediments (e.g. Yamazaki *et al.* 2003). Type b also shows the loss and partial recovery in SIRM, but there is a kink around 250 K which can be recognized as a discontinuity in the derivative curves (dotted lines in Fig. 3). Since the Morin transition temperature ( $T_M$ ) of haematite is around 260 K and it is lowered by Ti substitution (Dunlop & Özdemir 1997), and haematite particles of  $\leq 0.1 \ \mu m$ in size never show the transition (Bando *et al.* 1965), the present observation suggests the existence of a large amount of haematite associated with a small amount of Ti substitution. As a matter of fact, the corresponding two samples are reddish and contain a lot of heavily deuteric-oxidized olivine phenocrysts which are red in colour. The two Types a and b are yielded from samples with  $M_{s}$ -T curves of Types A and B, respectively, indicating consistent magnetic properties between low- and high-temperature magnetometry.

Types c, d and e show a common feature: a continuous decrease of the remanence at temperatures lower than 220 K in the cooling cycle, followed by a consecutive increase in the heating cycle. In Types d and e the curves are almost reversible and there is an additional kink around 220 K in Type e. Since all of them are observed from the samples with  $M_s$ -T curves of Types C, D, E and F, these lowtemperature properties may originate from Ti-rich titanomagnetite phases.

Table 1. Expe	rimenta	ıl result:	S ITOIII UIC	דוות-תוד	DIAW IIIVU	man int not														
Sample ID	ΗT	LT	$NRM_0$	$ARM0_0$	$B_{ m rc}/B_{ m c}$	$M_{ m \scriptscriptstyle IS}/M_{ m \scriptscriptstyle S}$	LTD	ļ	[	First heating				S	econd heatin	ß		$F_{\rm L}$	ц	ΔAIC
							(per cent)	$H_{\mathrm{L}}$	Slope $_{\rm A}$	Slope <sub>N</sub>	$f_{\rm N}$	$r_{ m N}$	$H_{\mathrm{L}}$	Slope $_{\rm A}$	Slope $_{\rm T}$	$f_{\mathrm{T}}$	$r_{\mathrm{T}}$	$(\mu T)$	$(\mu T)$	
Maupiti (16.44–.	16.4505	, 152.25	152.28° h	() 130	0.100	VOVEO	60	00	1 15	2117	0100	2000	c	2000	101	1 00	2000	0.01	L   K	0
MD01-04-1	<		7.01 167	001	7.100	0.2404	0.0	202	1.t 2.2	0.417	261.0	2000	D V	0200	10.1	0.000	C66.0	10.01	1.1/	0.1-
MP01-06-1	c		213	126			16.7	55	0 571	0.460	0 249	0800	n vr	0.822	266.0 81.1	0.886	0.987	10.0	C7. <b>H</b>	0.7
MP01-07-1			14.5	134			16.7	30	0.914	0.374	0.339	0.995	, vo	0.893	1.03	0.853	0.996	10.0	3.74	-1.9
MP01-09-1			12.2	108			25.4	20	0.423	0.396	0.301	0.980	0	0.999	0.973	1.00	0.993	10.0		
MP01-12-1			18.2	124			14.5	25	0.649	0.451	0.291	0.996	0	0.902	1.00	1.00	0.996	10.0	4.51	4.0
MP19-01-2			92.8	298			2.9	20	0.231	0.806	0.755	0.979	0	1.06	0.997	1.00	0.999	20.0		
MP19-02-1			91.1	290	1.375	0.5192	2.9	20	0.258	0.754	0.790	0.995	0	1.03	0.994	1.00	0.998	20.0	$15.1^{\rm a}$	2.3
MP19-04-2			68.0	260			2.9	30	0.165	0.763	0.639	0.995	0	1.06	0.996	1.00	0.999	20.0	$15.3^{\rm a}$	-1.7
MP19-05-1			75.5	283			3.8	25	0.254	1.12	0.721	0.995	0	1.01	1.01	1.00	0.999	10.0	$11.2^{a}$	5.6
MP19-06-1			69.4	243			-0.8	25	0.195	0.508	0.580	0.995	0	1.04	0.984	1.00	0.999	20.0	$10.2^{\mathrm{a}}$	9.9
MP19-07-1	Щ	c	67.4	226			4.8	25	0.179	0.662	0.684	0.995	0	1.06	0.997	1.00	0.996	20.0	<i>13.2</i> <sup>a</sup>	10.8
Borabora (16.46	-16.54°	S, 151.5	73-151.76°	(11)																
BR02-04-1	Щ	c	139	373	1.647	0.2447	6.5	10	0.393	0.999	0.662	0.995	40	1.02	1.04	0.723	0.995	10.0	$9.99^{a}$	7.2
BR02-05-1			138	362	1.648	0.2579	4.8	10	0.404	0.506	0.655	0.998	40	0.934	1.05	0.703	0.997	20.0	$10.1^{a}$	-1.7
BR02-06-1			133	385	1.630	0.2569	4.8	10	0.426	0.844	0.671	0.997	50	0.962	1.03	0.521	0.995	10.0	$8.44^{\mathrm{a}}$	-1.8
BR02-07-1			138	396	1.562	0.3050	3.8	10	0.406	0.958	0.998	0.750	45	1.04	1.05	0.620	0.995	10.0	$9.58^{a}$	0.7
BR08-01-2			467	255			2.0	15	0.191	2.44	0.805	0.995	10	1.08	0.888	1.00	0.999	20.0		
BR08-02-2w			767	345			-0.9	15	0.274	2.64	0.766	0.995	50	1.15	0.807	0.724	0.993	20.0		
BR08-03-1			164	190			6.5	5	0.225	0.849	0.994	0.984	0	1.18	0.869	1.00	0.998	20.0		
BR08-04-2			317	244			1.0	55	0.183	0.816	0.181	0.995	0	1.14	0.938	1.00	0.993	20.0		
BR08-05-1			1100	474			4.8	15	0.446	3.72	0.757	0.998	30	1.09	1.06	0.961	0.999	20.0		
BR08-06-1			985	494			4.8	15	0.510	3.59	0.723	0.998	0	1.00	1.10	1.00	0.998	20.0		
BR08-07-1			623	293			3.8	20	0.222	9.39	0.693	0.992	0	1.01	0.996	1.00	0.998	10.0		
BR09-03-1			148	274			9.1	5	0.885	0.352	0.687	0.975	10	0.842	1.00	0.861	0.998	40.0		
BR10-01-1			65.0	134	1.551	0.5325	7.4	55	0.545	0.248	0.275	0.991	0	0.831	1.05	1.00	0.996	20.0		
BR10-01-2			61.7	125	1.551	0.5325	3.8	65	0.621	0.500	0.232	0.996	0	0.826	1.04	1.00	0.997	10.0	$5.00^{\mathrm{b}}$	11.7
BR10-02-2			129	207			-2.4	40	1.25	1.97	0.486	0.995	0	0.834	0.913	1.00	0.995	5.00		
BR10-03-1	D	e	83.3	159	1.825	0.4486	-1.0	10	1.20	0.668	0.341	0.998	0	0.898	0.953	1.00	0.998	10.0	6.68 <sup>b</sup>	6.7
BR10-03-2	D	e	83.9	146	1.825	0.4486	2.0	55	1.33	0.761	0.403	0.992	0	0.852	0.912	1.00	0.995	10.0		
BR10-04-1			149	200	1.548	0.5002	5.7	55	0.972	0.806	0.226	0.996	0	0.834	1.12	1.00	0.998	10.0		
BR10-04-2			131	190	1.548	0.5002	-0.9	65	0.944	0.867	0.196	0.995	0	0.851	1.03	1.00	0.999	10.0	8.67 <sup>b</sup>	-1.9
BR 10-05-2			114	180			2.9	50	0.911	1.49	0.365	0.995	0	0.816	0.908	1.00	0.997	5.00		
BR10-07-2			78.1	147	1.615	0.5392	1.0	50	1.18	0.696	0.357	0.995	0	0.878	0.974	1.00	0.999	10.0	$6.96^{\mathrm{b}}$	17.1
BR16-01-2			230	348	1.669	0.3168	9.1	25	0.479	1.72	0.205	0.995	5	0.981	0.963	0.926	0.998	10.0	17.2 <sup>b</sup>	8.0
BR16-02-2			272	382	1.798	0.3268	4.8	25	0.446	0.765	0.214	0.995	0	0.980	1.03	1.00	0.999	20.0	$15.3^{\mathrm{b}}$	20.8
BR16-03-1	ц	p	269	361	1.882	0.2790	5.7	30	0.424	0.749	0.166	0.997	5	0.960	1.00	0.947	0.999	20.0	$15.0^{\rm b}$	2.1
BR16-04-1			110	297	2.274	0.3203	4.8	30	0.612	0.493	0.286	0.995	20	0.912	1.02	0.786	0.998	20.0	$9.86^{\mathrm{b}}$	2.1
BR16-05-1			85.7	232			16.7	10	0.463	1.22	0.738	0.996	20	0.902	1.12	0.883	0.998	10.0		
BR16-05-2			119	270			9.1	30	0.290	0.521	0.217	0.995	0	0.970	1.13	1.00	0.999	20.0		
BR16-06-1			255	366	1.705	0.3235	12.3	25	0.462	1.57	0.195	0.995	20	0.965	1.01	0.731	0.999	10.0	15.7 <sup>b</sup>	16.2
BR16-07-2			248	351			9.1	5	0.863	1.04	0.919	0.995	25	1.00	1.07	0.738	0.999	20.0		

| F AAIC      | (μT)             |                                    |          |                      |          | 10.2 21.3 |                |                              |                      |          |   |   |   |   |   | — — — — — — — — — — — — — — — — — — —  | $\begin{array}{c ccccccccccccccccccccccccccccccccccc$   | $\begin{array}{c ccccccccccccccccccccccccccccccccccc$  
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$F_{\rm L}$	(μT)
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   | 10.0           20.0  | 10.0           20.0  | 10.0           20.0  | 10.0           20.0  
   | 10.0           20.0   | 10.0           20.0  | 10.0           20.0   | 10.0           20.0           20.0           20.0           20.0           20.0          
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|             | $r_{\mathrm{T}}$ | 666.0 (                            | 966.0 6  | 8 0.996<br>0 0.996   | 1 0.996  | 666.0 (   | 866.0 (        | 2000                         |                      | 666.0 2  | 266-0 0<br>7 0.999<br>3 0.998           | 262.0 0<br>7 0.999<br>3 0.998<br>1 <i>9</i> 0.0 1 | 266.0 0<br>7 0.998<br>3 0.998<br>191.0 1<br>8 0.998 | 7         0.999           3         0.998           8         0.998           6         0.998 | 2000<br>3 0.998<br>8 0.998<br>8 0.998<br>3 0.996<br>3 0.996                                 | 6 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   | 3         0.999           3         0.999           8         0.998           6         0.999           3         0.999           0         0.999           3         0.999           3         0.999           5         0.999           3         0.999           3         0.999   | $\begin{array}{cccccccccccccccccccccccccccccccccccc$  | $\begin{array}{cccccccccccccccccccccccccccccccccccc$   | $\begin{array}{cccccccccccccccccccccccccccccccccccc$  | 7         0.9993           7         0.9994           8         0.9994           6         0.9993           3         0.9995           5         0.9995           3         0.9995           3         0.9995           9         0.9995           0         0.9995           0         0.9995           0         0.9995           0         0.9995           0         0.9995  
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| neating     | т <i>f</i> т     | 5 1.00                             | 0.66     | 8 0.708<br>0.810     | 0.79     | 0 1.00    | 5 1.00         | 002.0                        | 0.002                | ,96.0    | 0.96                                    | 0.96  | 0.960   | 0.96  | 0.967<br>0.707<br>0.707<br>0.753<br>0.750<br>0.750  | 0.967<br>0.532<br>0.703<br>0.888<br>0.888<br>0.750<br>0.750<br>1.000   | 0.967<br>0.533<br>0.533<br>0.756<br>0.776<br>0.677<br>0.677<br>0.665  | 0.96<br>0.53<br>0.70<br>0.75<br>0.75<br>0.67<br>0.67<br>0.67<br>0.67<br>0.66<br>0.66<br>0.66<br>0.66   
   | 0.967<br>0.753<br>0.775<br>0.756<br>0.756<br>0.677<br>0.667<br>0.667<br>0.667<br>0.662  | 0.96<br>0.53<br>0.70<br>0.75<br>0.75<br>0.67<br>0.67<br>0.67<br>0.67<br>0.66<br>0.66<br>0.90<br>0.90<br>0.90<br>0.90<br>0.90<br>0.90  | 0.96<br>0.73<br>0.73<br>0.73<br>0.75<br>0.75<br>0.75<br>0.75<br>0.75<br>0.75<br>0.75<br>0.75   | 0.96<br>0.73<br>0.73<br>0.73<br>0.75<br>0.75<br>0.67<br>0.67<br>0.67<br>0.66<br>0.84<br>0.90<br>0.1<br>0.09<br>0.0<br>0.1<br>0.00<br>0.1<br>0.00<br>0.1<br>0.00<br>0.10<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.000000 | 0.96<br>0.53<br>0.750<br>0.750<br>0.756<br>0.67<br>0.67<br>0.66<br>0.84<br>0.90<br>0.1<br>0.09<br>0.1<br>0.00<br>1.000<br>1.000<br>1.000<br>0.1  
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|             | Slope            | 0.930                              | 1.05     | 0.988<br>0.953       | 1.01     | 0.99(     | 0.976          | 101                          | 10.1                 | 1.1.1    | 1.22                                    | 1.22<br>1.08                                      | 1.22<br>1.08<br>1.00                                | 1.05<br>1.05<br>1.05  | 1.22<br>1.08<br>1.00<br>1.00<br>1.02  | 1.02<br>1.08<br>1.05<br>1.05<br>1.05   | 7.22<br>7.08<br>1.00<br>1.05<br>1.05<br>1.04<br>1.04<br>1.04  | <i>1.22</i><br><i>1.28</i><br><i>1.06</i><br><i>1.05</i><br><i>1.05</i><br><i>1.04</i><br><i>1.04</i><br><i>1.04</i>   
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7.27<br>7.08<br>1.00<br>1.01<br>1.02<br>1.02<br>1.03<br>1.04<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03<br>1.03 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1.00\\ 1.00\\$  | $\begin{array}{c} 1.00\\$  |
|             | Slope A          | 0.844                              | 0.945    | 0.868                | 0.877    | 1.00      | 0.895          | 001                          | c0.1<br>0.948        | 0000     | 0.808                                   | 0.733<br>0.733                                    | 0.808<br>0.733<br>0.864                             | 0.808<br>0.733<br>0.864<br>0.810  | 0.505<br>0.733<br>0.864<br>0.810<br>0.810   | 0.808<br>0.733<br>0.864<br>0.810<br>0.810<br>0.770<br>0.770  | 0.808<br>0.733<br>0.864<br>0.810<br>0.810<br>0.770<br>1.06<br>1.24  | 0.805<br>0.733<br>0.864<br>0.810<br>0.810<br>0.770<br>0.770<br>1.06<br>1.24<br>1.17  
   | 0.733<br>0.733<br>0.733<br>0.864<br>0.810<br>0.810<br>0.770<br>0.770<br>1.06<br>1.24<br>1.17  | 0.733<br>0.733<br>0.733<br>0.864<br>0.810<br>0.770<br>0.770<br>1.06<br>1.17<br>1.11<br>1.11   | 0.805<br>0.733<br>0.733<br>0.864<br>0.810<br>0.770<br>0.770<br>0.770<br>1.06<br>1.17<br>1.17<br>1.11<br>1.11<br>1.11<br>1.11<br>1.11<br>1.1  | 0.805<br>0.733<br>0.733<br>0.864<br>0.810<br>0.770<br>0.770<br>0.770<br>1.06<br>1.17<br>1.11<br>1.11<br>1.11<br>1.11<br>1.11<br>1.11<br>1.1   | 0.805<br>0.733<br>0.864<br>0.810<br>0.810<br>0.770<br>0.770<br>0.770<br>1.06<br>1.17<br>1.11<br>1.11<br>1.11<br>1.11<br>1.11<br>1.11<br>1.1  
   | 0.805<br>0.733<br>0.864<br>0.810<br>0.810<br>0.770<br>0.810<br>0.770<br>1.05<br>1.17<br>1.11<br>1.11<br>1.11<br>1.11<br>1.11<br>1.11<br>1.1  | 0.805<br>0.733<br>0.864<br>0.810<br>0.810<br>0.770<br>0.770<br>0.770<br>1.06<br>1.17<br>1.11<br>1.11<br>1.11<br>1.11<br>1.11<br>1.11<br>1.1  | 0.805<br>0.733<br>0.864<br>0.810<br>0.810<br>0.810<br>0.810<br>0.770<br>0.810<br>1.05<br>1.17<br>1.11<br>1.11<br>1.11<br>1.12<br>1.25<br>1.05<br>1.125<br>1.04<br>1.142<br>1.142<br>1.142<br>1.142<br>1.142  | 0.805<br>0.733<br>0.864<br>0.810<br>0.810<br>0.770<br>0.770<br>0.770<br>1.06<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.1  
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   | 0.805<br>0.733<br>0.864<br>0.770<br>0.770<br>0.770<br>0.770<br>1.03<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.03<br>1.04<br>1.142<br>1.04<br>1.04<br>1.04<br>1.04<br>1.04<br>1.04<br>1.04<br>1.04   | 0.800<br>0.733<br>0.864<br>0.730<br>0.770<br>0.770<br>0.770<br>1.06<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.142<br>1.05<br>1.04<br>1.04<br>1.04<br>1.04<br>1.04<br>1.04<br>1.04<br>1.04  | 0.733<br>0.864<br>0.733<br>0.864<br>0.810<br>0.770<br>0.770<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17  
   | 0.733<br>0.864<br>0.733<br>0.864<br>0.810<br>0.770<br>0.770<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17   
  | 0.733<br>0.864<br>0.733<br>0.864<br>0.770<br>0.770<br>1.06<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.04<br>1.04<br>1.04<br>1.04<br>1.04<br>1.04<br>1.04<br>1.04  | 0.500<br>0.733<br>0.864<br>0.770<br>0.770<br>0.770<br>0.770<br>0.770<br>1.06<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.16<br>1.16<br>1.16<br>1.04<br>1.04<br>1.04<br>1.04<br>1.04<br>1.05<br>1.06<br>1.06<br>1.06<br>1.07<br>1.06<br>1.07<br>1.06<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07<br>1.07   |
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|             | $r_{\rm N}$      | 0 0.90                             | 0 0.95   | 0 0.93<br>0 0.93     | 0 0.95   | 1 0.99    | 0 0.97         | 000                          | 1 0.90<br>9 0.97     |          | 2 0.99                                  | 2 0.99<br>2 0.99                                  | 2 0.99<br>2 0.99                                    | 2 0.99<br>2 0.99  | 2 0.99<br>3 0.99<br>3 0.99  | 2 0.99<br>2 0.99<br>3 0.99<br>3 0.99   | 2         0.99           2         0.99           3         0.99           3         0.99           5         0.99  | 2         0.99           2         0.99           3         0.99           3         0.99           3         0.99           1         0.99  
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   |
|             | $f_{\rm N}$      | 0.086                              | 0.068    | 0.086<br>0.090       | 0.090    | 0.35      | 0.12(          | 010                          | 0.420                |          | 0.602                                   | 0.602<br>0.542                                    | 0.602<br>0.542<br>omponent                          | 0.602<br>0.542<br>omponent<br>0.533   | 0.600<br>0.542<br>0.542<br>0.533<br>0.362   | 0.602<br>0.542<br>0.542<br>0.537<br>0.562<br>0.562   | 0.60<br>0.54<br>0.53<br>0.53<br>0.36<br>0.56<br>0.88  | 0.602<br>0.542<br>0.542<br>0.553<br>0.553<br>0.553<br>0.567<br>0.567<br>0.582<br>0.882   
   | 0.602<br>0.542<br>0.542<br>0.533<br>0.563<br>0.565<br>0.565<br>0.912<br>0.912   | 0.602<br>0.542<br>0.533<br>0.533<br>0.565<br>0.565<br>0.565<br>0.911<br>0.911<br>0.912  | 0.602<br>0.542<br>0.553<br>0.365<br>0.365<br>0.365<br>0.565<br>0.882<br>0.565<br>0.912<br>0.912<br>0.882<br>0.912<br>0.912<br>0.912<br>0.765 | 0.607<br>0.547<br>0.547<br>0.567<br>0.567<br>0.567<br>0.567<br>0.567<br>0.567<br>0.267<br>0.177<br>0.777  | 0.607<br>0.547<br>0.547<br>0.567<br>0.567<br>0.567<br>0.567<br>0.567<br>0.911<br>0.776<br>0.776<br>0.776<br>0.776<br>0.776   
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   | 0.547<br>0.547<br>0.547<br>0.567<br>0.266<br>0.911<br>0.177<br>0.177<br>0.177<br>0.177<br>0.177<br>0.156<br>0.156<br>0.157<br>0.157<br>0.157<br>0.157<br>0.156<br>0.157<br>0.667<br>0.667<br>0.664  | 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| Clone .     | V odore          | 0.179                              | 0.377    | 0.461                | 0.559    | 1.02      | 0.478          | 200.0                        | 0.907                |          | 0.976                                   | 0.976<br>0.649                                    | 0.976<br>0.649<br>0.649<br>primary co               | 0.976<br>0.649<br>primary ce<br>1.73  | 0.976<br>0.649<br>0.649<br>1.73<br>1.73<br>1.49   | 0.976<br>0.649<br>0.649<br>1.73<br>1.73<br>0.629   | 0.976<br>0.649<br>0.649<br>1.73<br>1.49<br>0.629<br>0.575   | 0.976<br>0.649<br>0.649<br>1.73<br>1.73<br>1.73<br>0.629<br>0.629<br>0.575<br>1.23   
   | 0.976<br>0.649<br>0.649<br>1.73<br>1.73<br>1.73<br>0.629<br>0.629<br>1.23<br>1.23   | 0.976<br>0.649<br>0.649<br>1.73<br>1.49<br>0.629<br>0.629<br>1.23<br>1.23<br>1.23<br>1.23<br>1.87<br>0.575<br>0.575   | 0.976<br>0.649<br>1.73<br>1.74<br>1.749<br>0.629<br>0.629<br>0.575<br>1.23<br>1.23<br>1.23<br>1.23<br>0.721<br>2.84<br>0.803                 | 0.976<br>0.649<br>0.649<br>1.73<br>1.49<br>0.629<br>0.575<br>1.23<br>1.87<br>0.575<br>1.23<br>1.87<br>0.575<br>0.575<br>0.575<br>0.575<br>0.721<br>0.721<br>0.721<br>0.723  | 0.976<br>0.649<br>1.73<br>1.73<br>1.49<br>0.629<br>0.629<br>1.23<br>1.23<br>1.23<br>0.721<br>2.84<br>0.373<br>0.721<br>0.575   
   | 0.976<br>0.649<br>1.73<br>1.73<br>1.49<br>0.629<br>0.629<br>0.629<br>1.49<br>0.575<br>1.23<br>1.87<br>0.721<br>2.84<br>0.373<br>0.174<br>0.251<br>0.251  | 0.976<br>0.649<br>1.73<br>1.73<br>1.49<br>0.629<br>0.629<br>0.629<br>1.23<br>1.23<br>1.23<br>1.23<br>0.721<br>2.84<br>0.721<br>2.84<br>0.721<br>0.771<br>0.775<br>0.2551<br>0.101  | 0.976<br>0.649<br>1.73<br>1.73<br>1.49<br>0.629<br>0.629<br>0.629<br>1.23<br>1.23<br>1.23<br>1.23<br>0.721<br>2.84<br>0.721<br>2.84<br>0.721<br>0.775<br>0.275<br>0.275  | 0.976<br>0.649<br>1.73<br>1.73<br>1.49<br>0.629<br>0.629<br>0.629<br>1.49<br>0.575<br>1.23<br>1.23<br>1.23<br>0.721<br>0.721<br>0.255<br>0.212<br>0.212<br>0.744   
   | 0.976<br>0.649<br>0.649<br>1.73<br>1.49<br>0.629<br>0.575<br>1.23<br>1.87<br>0.575<br>0.744<br>0.717<br>0.7174<br>0.101<br>0.255<br>0.251<br>0.714<br>0.572<br>0.572<br>0.572<br>0.572  | 0.976<br>0.649<br>1.73<br>1.49<br>0.629<br>0.575<br>1.49<br>0.575<br>1.23<br>1.87<br>0.575<br>0.575<br>0.575<br>0.251<br>0.101<br>0.101<br>0.252<br>0.2517<br>0.251<br>0.522<br>0.517<br>0.522<br>0.517  | 0.976<br>0.649<br>1.73<br>1.49<br>0.629<br>0.575<br>1.49<br>0.575<br>1.23<br>1.87<br>0.575<br>0.575<br>0.575<br>0.575<br>0.717<br>0.717<br>0.712<br>0.712<br>0.712<br>0.712<br>0.721<br>0.721<br>0.721<br>0.721<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.7577<br>0.7577<br>0.7577<br>0.7577<br>0.7577<br>0.7577<br>0.7577<br>0.7577<br>0.7577<br>0.7577<br>0.7577<br>0.7577<br>0.7577<br>0.7577<br>0.75777<br>0.7577<br>0.7577<br>0.7577<br>0.7577<br>0.75777<br>0.75777<br>0.75777<br>0.75777<br>0.75777<br>0.757777777777   |
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0.976<br>0.649<br>1.73<br>1.73<br>1.49<br>0.629<br>0.629<br>0.575<br>0.575<br>1.257<br>0.575<br>0.575<br>0.575<br>0.257<br>0.703<br>0.704<br>0.212<br>0.212<br>0.287<br>0.212<br>0.287<br>0.2617<br>1.40<br>0.703<br>1.40<br>0.703<br>1.20<br>0.517<br>1.40<br>0.703<br>0.517<br>1.40<br>0.703<br>0.517<br>1.40<br>0.522<br>0.557<br>0.557<br>0.557<br>0.557<br>0.557<br>0.557<br>0.557<br>0.557<br>0.557<br>0.557<br>0.557<br>0.557<br>0.557<br>0.557<br>0.557<br>0.557<br>0.557<br>0.557<br>0.557<br>0.557<br>0.557<br>0.557<br>0.557<br>0.557<br>0.557<br>0.557<br>0.557<br>0.557<br>0.557<br>0.557<br>0.557<br>0.557<br>0.557<br>0.557<br>0.557<br>0.557<br>0.557<br>0.557<br>0.557<br>0.557<br>0.557<br>0.557<br>0.557<br>0.557<br>0.557<br>0.557<br>0.557<br>0.557<br>0.557<br>0.557<br>0.557<br>0.557<br>0.557<br>0.557<br>0.557<br>0.557<br>0.557<br>0.557<br>0.557<br>0.557<br>0.557<br>0.557<br>0.557<br>0.557<br>0.557<br>0.557<br>0.557<br>0.557<br>0.557<br>0.557<br>0.557<br>0.557<br>0.557<br>0.557<br>0.557<br>0.557<br>0.557<br>0.557<br>0.557<br>0.557<br>0.557<br>0.557<br>0.557<br>0.557<br>0.557<br>0.557<br>0.557<br>0.557<br>0.557<br>0.557<br>0.557<br>0.557<br>0.557<br>0.557<br>0.557<br>0.557<br>0.557<br>0.557<br>0.557<br>0.557<br>0.557<br>0.557<br>0.557<br>0.557<br>0.557<br>0.557<br>0.557<br>0.557<br>0.5577<br>0.5577<br>0.5577<br>0.5577<br>0.5577<br>0.5577<br>0.5577<br>0.5577<br>0.5577<br>0.5577<br>0.5577<br>0.5577<br>0.5577<br>0.5577<br>0.5577<br>0.5577<br>0.5577<br>0.5577<br>0.5577<br>0.5577<br>0.5577<br>0.5577<br>0.5577<br>0.5577<br>0.5577<br>0.5577<br>0.5577<br>0.5577<br>0.5577<br>0.5577<br>0.5577<br>0.5577<br>0.5577<br>0.5577<br>0.5577<br>0.5577<br>0.5577<br>0.5577<br>0.5577<br>0.5577<br>0.5577<br>0.5577<br>0.5577<br>0.5577<br>0.5577<br>0.5577<br>0.5577<br>0.5577<br>0.5577<br>0.5577<br>0.5577<br>0.5577<br>0.5577<br>0.5577<br>0.5577<br>0.5577<br>0.5577<br>0.5577<br>0.5577<br>0.5577<br>0.5577<br>0.5577<br>0.5577<br>0.5577<br>0.5577<br>0.5577<br>0.5577<br>0.5577<br>0.5577<br>0.55770<br>0.55770<br>0.55770<br>0.55770<br>0.55770<br>0.55770<br>0.557700<br>0.557700<br>0.557700<br>0.55770000000000  | 0.976<br>0.649<br>0.649<br>0.629<br>0.629<br>0.575<br>0.575<br>0.575<br>0.575<br>0.575<br>0.575<br>0.257<br>0.703<br>0.174<br>0.108<br>0.517<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.297<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.297<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.297<br>0.287<br>0.297<br>0.297<br>0.297<br>0.297<br>0.297<br>0.297<br>0.297<br>0.297<br>0.297<br>0.297<br>0.29700000000000000000000000000000000000  |
| Clano       | V adore          | 0.558                              | 0.355    | 0.385<br>0.441       | 0.366    | 0.605     | 0.451          | 0200                         | 0.173                |          | 0.382                                   | 0.382 0.317                                       | 0.382<br>0.382<br>0.317<br>No                       | 0.292<br>0.292<br>0.292   | 0.317<br>0.317<br>No<br>0.292<br>0.287  | 0.1145<br>0.382<br>0.317<br>No<br>0.292<br>0.287<br>0.287  | 0.342<br>0.317<br>0.317<br>0.322<br>0.292<br>0.287<br>0.542<br>0.542  | 0.342<br>0.317<br>0.317<br>0.287<br>0.287<br>0.287<br>0.542<br>0.542<br>0.332  
   | $\begin{array}{c} 0.342\\ 0.317\\ 0.317\\ 0.287\\ 0.287\\ 0.542\\ 0.542\\ 0.332\\ 0.332\\ 0.239\\ 0.239\\ 0.239\end{array}$   | 0.317<br>0.317<br>No<br>0.287<br>0.542<br>0.542<br>0.332<br>0.333<br>0.233  | 0.317<br>0.317<br>0.317<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.332<br>0.332<br>0.239<br>0.239                                     | 0.317<br>0.317<br>0.317<br>0.287<br>0.287<br>0.287<br>0.287<br>0.239<br>0.332<br>0.239<br>0.239<br>0.239<br>0.239   | 0.347<br>0.317<br>0.317<br>0.317<br>0.287<br>0.287<br>0.287<br>0.287<br>0.332<br>0.239<br>0.239<br>0.236<br>0.236  
   | 0.317<br>0.317<br>0.317<br>0.317<br>0.340<br>0.542<br>0.332<br>0.332<br>0.332<br>0.239<br>0.236<br>0.236<br>0.236<br>0.236<br>0.236<br>0.236<br>0.236<br>0.236<br>0.236<br>0.236<br>0.237<br>0.237<br>0.237<br>0.237<br>0.237<br>0.240<br>0.237<br>0.267<br>0.267<br>0.267<br>0.267<br>0.267<br>0.267<br>0.267<br>0.267<br>0.267<br>0.267<br>0.267<br>0.267<br>0.267<br>0.267<br>0.267<br>0.267<br>0.267<br>0.267<br>0.267<br>0.267<br>0.267<br>0.267<br>0.267<br>0.267<br>0.267<br>0.267<br>0.267<br>0.267<br>0.267<br>0.267<br>0.267<br>0.267<br>0.267<br>0.267<br>0.267<br>0.267<br>0.267<br>0.267<br>0.267<br>0.267<br>0.267<br>0.267<br>0.267<br>0.267<br>0.267<br>0.267<br>0.267<br>0.267<br>0.267<br>0.267<br>0.267<br>0.267<br>0.267<br>0.267<br>0.267<br>0.267<br>0.267<br>0.267<br>0.267<br>0.267<br>0.267<br>0.267<br>0.267<br>0.267<br>0.267<br>0.2767<br>0.2767<br>0.2767<br>0.2767<br>0.2767<br>0.2767<br>0.2767<br>0.2767<br>0.2767<br>0.2767<br>0.2767<br>0.2767<br>0.2767<br>0.2766<br>0.2766<br>0.2766<br>0.2766<br>0.2766<br>0.2766<br>0.2766<br>0.2766<br>0.2766<br>0.2766<br>0.2766<br>0.2766<br>0.2766<br>0.2766<br>0.2766<br>0.2766<br>0.2766<br>0.2766<br>0.2766<br>0.2766<br>0.2766<br>0.2766<br>0.2066<br>0.2066<br>0.2066<br>0.2066<br>0.2066<br>0.2066<br>0.2066<br>0.2066<br>0.2066<br>0.2066<br>0.2066<br>0.2066<br>0.2066<br>0.2066<br>0.2066<br>0.2066<br>0.2066<br>0.2066<br>0.2066<br>0.2066<br>0.2066<br>0.2066<br>0.2066<br>0.2066<br>0.2066<br>0.2066<br>0.2066<br>0.2066<br>0.2066<br>0.2066<br>0.2066<br>0.2066<br>0.2066<br>0.2066<br>0.2066<br>0.2066<br>0.2066<br>0.2066<br>0.2066<br>0.2066<br>0.2066<br>0.2066<br>0.2066<br>0.2066<br>0.2066<br>0.2066<br>0.2066<br>0.2066<br>0.2066<br>0.2066<br>0.2066<br>0.2066<br>0.2066<br>0.2066<br>0.2066<br>0.2066<br>0.2066<br>0.2066<br>0.2066<br>0.2066<br>0.2066<br>0.2066<br>0.2066<br>0.2066<br>0.2066<br>0.2066<br>0.2066<br>0.2066<br>0.2066<br>0.2066<br>0.2066<br>0.2066<br>0.2066<br>0.2066<br>0.2066<br>0.2066<br>0.2066<br>0.2066<br>0.2066<br>0.2066<br>0.2066<br>0.2066<br>0.2066<br>0.2066<br>0.2066<br>0.2066<br>0.2066<br>0.2066<br>0.2066<br>0.2066<br>0.2066<br>0.2066<br>0.2066<br>0.2066<br>0.2066<br>0.2066<br>0.2066<br>0.2066<br>0.2066<br>0.2066<br>0.2066<br>0.2066<br>0.2066<br>0.2066<br>0.2066<br>0.2066<br>0.2066<br>0.2066<br>0.2066<br>0.2066<br>0.2066<br>0.2066<br>0.2066<br>0.2066<br>0.2066<br>0.2066<br>0.2066<br>0.2066<br>0.2066<br>0.2066<br>0.2066<br>0.2066<br>0.2066<br>0.2066<br>0.2066<br>0.2066<br>0.2066<br>0.2066<br>0.2066<br>0.2066<br>0.2066<br>0.2066<br>0.2066<br>0.2066<br>0.2066<br>0.2066<br>0.2066<br>0.2066<br>0.2066<br>0.2066<br>0.   | 0.317<br>No<br>0.317<br>0.317<br>0.317<br>0.287<br>0.287<br>0.542<br>0.332<br>0.332<br>0.332<br>0.332<br>0.332<br>0.332<br>0.332<br>0.332<br>0.332<br>0.332<br>0.332<br>0.236<br>0.418<br>0.475  | 0.317<br>0.317<br>0.317<br>0.317<br>0.287<br>0.287<br>0.542<br>0.542<br>0.542<br>0.332<br>0.332<br>0.239<br>0.236<br>0.236<br>0.236<br>0.236<br>0.236<br>0.236<br>0.236<br>0.236<br>0.236<br>0.236<br>0.237<br>0.337   | 0.317<br>No<br>0.317<br>0.317<br>0.287<br>0.287<br>0.287<br>0.332<br>0.332<br>0.333<br>0.333<br>0.475<br>0.337<br>0.475<br>0.337   
   | 0.317<br>No<br>0.317<br>0.317<br>0.287<br>0.542<br>0.542<br>0.544<br>0.333<br>0.333<br>0.296<br>0.296<br>0.333<br>0.296<br>0.3337<br>0.475<br>0.337<br>0.475<br>0.475<br>0.475<br>0.446   | 0.317<br>No<br>0.317<br>0.317<br>0.327<br>0.542<br>0.542<br>0.544<br>0.333<br>0.276<br>0.296<br>0.296<br>0.296<br>0.296<br>0.296<br>0.3337<br>0.2555<br>0.3337<br>0.418<br>0.418<br>0.429<br>0.439   | 0.2475<br>0.317<br>0.317<br>0.317<br>0.287<br>0.287<br>0.542<br>0.542<br>0.542<br>0.333<br>0.296<br>0.296<br>0.296<br>0.296<br>0.296<br>0.296<br>0.296<br>0.296<br>0.296<br>0.296<br>0.296<br>0.296<br>0.296<br>0.297<br>0.296<br>0.297<br>0.298<br>0.298<br>0.298<br>0.298<br>0.298<br>0.298<br>0.298<br>0.298<br>0.298<br>0.298<br>0.298<br>0.298<br>0.298<br>0.298<br>0.298<br>0.298<br>0.298<br>0.298<br>0.2987<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.287<br>0.276<br>0.2766<br>0.2766<br>0.2776<br>0.2373<br>0.2776<br>0.2373<br>0.2776<br>0.2470<br>0.2475<br>0.2475<br>0.2475<br>0.2475<br>0.2475<br>0.2475<br>0.2475<br>0.2475<br>0.2475<br>0.2475<br>0.2475<br>0.2475<br>0.2475<br>0.2475<br>0.2475<br>0.2475<br>0.2475<br>0.2475<br>0.2475<br>0.2475<br>0.2475<br>0.2475<br>0.2475<br>0.2475<br>0.2475<br>0.2475<br>0.2475<br>0.2475<br>0.2475<br>0.2475<br>0.2475<br>0.2475<br>0.2475<br>0.2475<br>0.2475<br>0.2475<br>0.2475<br>0.2475<br>0.2475<br>0.2475<br>0.2475<br>0.2475<br>0.2475<br>0.2475<br>0.2475<br>0.2475<br>0.2475<br>0.2475<br>0.2475<br>0.2475<br>0.2475<br>0.2475<br>0.2475<br>0.2475<br>0.2475<br>0.2475<br>0.2475<br>0.2475<br>0.2475<br>0.2475<br>0.2475<br>0.2475<br>0.2475<br>0.2475<br>0.2475<br>0.2475<br>0.2475<br>0.2475<br>0.2475<br>0.2475<br>0.2475<br>0.2475<br>0.2475<br>0.2475<br>0.2475<br>0.2475<br>0.2475<br>0.2475<br>0.2475<br>0.2475<br>0.2475<br>0.2475<br>0.2475<br>0.2475<br>0.2475<br>0.2475<br>0.2475<br>0.2475<br>0.2475<br>0.2475<br>0.2475<br>0.2475<br>0.2475<br>0.2475<br>0.2475<br>0.2475<br>0.2475<br>0.2475<br>0.2475<br>0.2475<br>0.2475<br>0.2475<br>0.2475<br>0.2475<br>0.2475<br>0.2475<br>0.2475<br>0.2475<br>0.2475<br>0.2475<br>0.2475<br>0.2475<br>0.2475<br>0.2475<br>0.2475<br>0.2475<br>0.2475<br>0.2475<br>0.2475<br>0.2475<br>0.2475<br>0.2475<br>0.2475<br>0.2475<br>0.2475<br>0.2475<br>0.2475<br>0.2475<br>0.2475<br>0.2475<br>0.2475<br>0.2475<br>0.2475<br>0.2475<br>0.2475<br>0.2475<br>0.2475<br>0.2475<br>0.2475<br>0.2475<br>0.2475<br>0.2475<br>0.2475<br>0.2475<br>0.2475<br>0.2475<br>0.2475<br>0.2475<br>0.2475<br>0.2475<br>0.2475<br>0.2475<br>0.2475<br>0.2475<br>0.2475<br>0.2475<br>0.24750<br>0.24750<br>0.24750<br>0.24750<br>0.24750<br>0.2475000000000000000000000000000000000000   |
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|             | $H_{\mathrm{L}}$ | 20                                 | 20       | 20<br>20             | 20       | 15        | 20             | 00                           | 20                   | 1        | 15                                      | 15  | 15<br>15  | 15<br>15<br>20  | 15<br>15<br>20<br>20  | 15<br>15<br>20<br>20<br>20   | 15<br>15<br>20<br>20<br>10  | 15<br>15<br>20<br>20<br>20<br>10   
   | 15<br>16<br>20<br>20<br>20<br>20<br>20<br>10<br>10  | 15<br>15<br>20<br>20<br>20<br>10<br>15<br>15<br>55  | 15<br>20<br>20<br>20<br>20<br>10<br>15<br>15<br>15<br>15   | 15<br>15<br>20<br>20<br>20<br>20<br>10<br>15<br>15<br>10  | 15<br>15<br>20<br>20<br>20<br>10<br>15<br>15<br>10<br>15<br>15<br>10<br>15<br>10<br>10   
   | 15<br>15<br>20<br>20<br>20<br>20<br>10<br>15<br>15<br>10<br>10<br>10   | 15<br>15<br>20<br>20<br>20<br>20<br>10<br>15<br>15<br>10<br>10<br>10<br>0<br>0   | 15<br>15<br>20<br>20<br>20<br>20<br>10<br>10<br>15<br>15<br>10<br>10<br>10<br>10<br>10<br>20<br>20<br>20<br>20<br>20<br>20<br>20<br>20<br>20<br>20<br>20<br>20<br>20   | 15<br>16<br>16<br>10<br>10<br>10<br>10<br>10<br>10<br>10<br>10<br>10<br>10<br>10<br>10<br>10   
   | 15<br>20<br>20<br>20<br>20<br>20<br>20<br>20<br>20<br>20<br>20<br>20<br>20<br>20  | 15<br>15<br>20<br>20<br>10<br>10<br>10<br>10<br>10<br>10<br>10<br>10<br>20<br>20<br>20<br>20<br>20<br>20<br>20<br>20<br>20<br>20<br>20<br>20<br>20   | 15<br>20<br>20<br>20<br>10<br>10<br>10<br>10<br>10<br>10<br>10<br>10<br>10<br>10<br>10<br>10<br>10  | 15<br>20<br>20<br>20<br>20<br>20<br>20<br>20<br>20<br>20<br>20<br>20<br>20<br>20           
   | 15<br>15<br>10<br>10<br>10<br>10<br>10<br>10<br>10<br>10<br>10<br>10<br>10<br>10<br>10  | 15<br>20<br>20<br>20<br>20<br>20<br>20<br>20<br>20<br>20<br>20<br>20<br>20<br>20  
   | 15<br>20<br>20<br>20<br>20<br>20<br>20<br>20<br>20<br>20<br>20<br>20<br>20<br>20   | 15<br>15<br>10<br>10<br>10<br>10<br>10<br>10<br>10<br>10<br>10<br>10<br>10<br>10<br>10   | 15<br>20<br>20<br>20<br>20<br>20<br>20<br>20<br>20<br>20<br>20<br>20<br>20<br>20  | $\begin{array}{cccccccccccccccccccccccccccccccccccc$  
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   | 15<br>20<br>20<br>20<br>20<br>20<br>20<br>20<br>20<br>20<br>20<br>20<br>20<br>20  
  | 15<br>20<br>20<br>20<br>20<br>20<br>20<br>20<br>20<br>20<br>20<br>20<br>20<br>20  | 15<br>15<br>16<br>17<br>10<br>10<br>10<br>10<br>10<br>10<br>10<br>10<br>10<br>10<br>10<br>10<br>10   | 15<br>20<br>20<br>20<br>20<br>20<br>20<br>20<br>20<br>20<br>20<br>20<br>20<br>20  
   | $\begin{array}{cccccccccccccccccccccccccccccccccccc$  | $\begin{array}{cccccccccccccccccccccccccccccccccccc$  
   |
|             | (per cent)       | 20.6                               | 18.0     | 16.7<br>17.4         | 16.0     | 15.3      | 19.4           | 0                            | 5.0<br>0.0           | 27.5     | ;;;;;;;;;;;;;;;;;;;;;;;;;;;;;;;;;;;;;;; | 31.5  | 31.5<br>20.6  | 31.5<br>20.6<br>22.5  | 31.5<br>20.6<br>31.5<br>31.5  | 31.5<br>31.5<br>20.6<br>31.5<br>11.5   | 31.5<br>20.6<br>31.5<br>22.5<br>31.5<br>11.5<br>2.0   | 31.5<br>20.6<br>31.5<br>31.5<br>11.5<br>22.0<br>2.0  
   | 31.5<br>20.6<br>31.5<br>31.5<br>31.5<br>22.5<br>22.5<br>22.0<br>2.0<br>2.0<br>2.0<br>2.0  | 31.5<br>22.5<br>31.5<br>31.5<br>22.6<br>2.0<br>2.0<br>2.0<br>2.0<br>2.0<br>2.0  | 31.5<br>22.5<br>31.5<br>31.5<br>22.6<br>22.6<br>2.0<br>2.0<br>2.0<br>2.0<br>2.0<br>2.0   | 31.5<br>22.5<br>31.5<br>22.5<br>22.5<br>22.6<br>2.0<br>2.0<br>2.0<br>2.0<br>2.0<br>2.0<br>2.0<br>2.0  | 31.5<br>22.5<br>31.5<br>22.5<br>22.5<br>22.5<br>2.0<br>2.0<br>2.0<br>2.0<br>2.0<br>2.0<br>0.0  
   | 31.5<br>22.5<br>31.5<br>22.5<br>22.6<br>2.0<br>2.0<br>2.0<br>2.0<br>2.0<br>2.0<br>2.0<br>2.0   | 31.5<br>22.5<br>31.5<br>22.5<br>22.6<br>2.0<br>2.0<br>2.0<br>2.0<br>2.0<br>2.0<br>2.0<br>3.8<br>3.8  | 31.5<br>22.5<br>31.5<br>22.5<br>22.5<br>2.0<br>2.0<br>2.0<br>2.0<br>2.0<br>2.0<br>2.0<br>2.0<br>2.0<br>2.0   | 20.6<br>20.6<br>21.5<br>21.5<br>2.16<br>2.0<br>2.0<br>2.0<br>2.0<br>2.0<br>2.0<br>2.0<br>2.0<br>2.0<br>2.0   
   | 22.5<br>21.5<br>21.5<br>21.9<br>22.6<br>22.0<br>22.0<br>22.0<br>22.0<br>22.0<br>22.0<br>22.0  | 22.5<br>21.5<br>21.5<br>21.5<br>22.5<br>22.5<br>2.0<br>2.0<br>2.9<br>2.0<br>2.9<br>2.0<br>2.9<br>2.0<br>2.0<br>2.0<br>2.0<br>2.0<br>2.0<br>2.0<br>2.0<br>2.0<br>2.0  | 31.5<br>22.5<br>31.5<br>22.5<br>22.5<br>2.0<br>2.0<br>2.0<br>2.0<br>2.0<br>2.0<br>2.0<br>2.0<br>2.0<br>2.0  |
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   | 22.5<br>21.5<br>22.5<br>21.5<br>22.5<br>22.5<br>22.0<br>22.0<br>22.0<br>22.0<br>22.0<br>22   | 22.5<br>21.5<br>22.5<br>21.5<br>22.5<br>22.5<br>22.0<br>22.0<br>22.0<br>22.0<br>22.0<br>22   | 20.6<br>20.6<br>21.5<br>20.6<br>22.5<br>20.6<br>22.0<br>22.0<br>22.0<br>22.0<br>22.0<br>22.0<br>22.0  | 31.5<br>20.6<br>21.5<br>21.5<br>21.5<br>22.6<br>22.0<br>22.0<br>22.0<br>22.0<br>22.0<br>22.0<br>22.0  
   | 31.5<br>20.6<br>21.5<br>21.5<br>21.5<br>22.6<br>22.0<br>22.0<br>22.0<br>22.0<br>22.0<br>22.0<br>22.0   | $\begin{array}{c} 3.1.5\\ 2.$   |
31.5<br>20.6<br>21.5<br>21.5<br>21.5<br>22.6<br>22.0<br>22.9<br>22.0<br>22.9<br>22.0<br>22.9<br>22.0<br>22.9<br>22.0<br>22.9<br>22.0<br>22.9<br>22.0<br>22.9<br>22.0<br>22.9<br>22.0<br>22.9<br>22.0<br>22.0   | $\begin{array}{c} 3.1.5\\ 2.1.5\\
2.1.5\\ 2.$  | $\begin{array}{c} 3.15\\ 2.15\\ 2.15\\ 2.15\\ 2.15\\ 2.15\\ 2.16\\ 2.19\\$  | $\begin{array}{c} 3.15\\ 2.15\\ 2.15\\ 2.15\\ 2.15\\ 2.15\\ 2.15\\ 2.16\\$   | $\begin{array}{c} 3.15\\ 2.15\\ 2.15\\ 2.15\\ 2.15\\ 2.15\\ 2.16\\
2.16\\ 2.16\\$  | 20.6<br>20.6<br>21.5<br>21.5<br>21.5<br>22.5<br>22.6<br>22.0<br>22.0<br>22.0<br>22.0<br>22.0<br>22.0<br>22.0  | 20.6<br>20.6<br>20.5<br>20.5<br>20.6<br>20.6<br>20.6<br>20.6<br>20.6<br>20.6<br>20.6<br>20.6   
  |
|             |                  |                                    |          |                      |          | 0.1503    |                |                              | 0.1924               |          |   |   |   | 0.1532  | 0.1532  | $\begin{array}{c}\\ 0.1532\\ 0.1539\\ 0.2892\end{array}$   | $\begin{array}{c}\\ 0.1532\\ 0.1539\\ 0.2892\\ 0.3821 \end{array}$  | $\begin{array}{c} & & \\$   
   | 0.1532<br>0.1539<br>0.2892<br>0.3821<br>0.4280<br>0.3826  | 0.1532<br>0.1539<br>0.2892<br>0.3821<br>0.4280<br>0.3826<br>0.3826<br>0.5803  | 0.1532<br>0.1539<br>0.2892<br>0.2822<br>0.3821<br>0.4280<br>0.5803<br>0.5803   | 0.1532<br>0.1539<br>0.2892<br>0.2892<br>0.2803<br>0.4820<br>0.5803<br>0.4832<br>0.4832<br>0.4832  | 0.1532<br>0.1539<br>0.2892<br>0.3821<br>0.3821<br>0.4280<br>0.3826<br>0.3826<br>0.5803<br>0.4832<br>0.3633   
   | 0.1532<br>0.1539<br>0.2892<br>0.3821<br>0.3821<br>0.4280<br>0.3826<br>0.5803<br>0.4832<br>0.4832   | 0.1532<br>0.1539<br>0.1539<br>0.2892<br>0.2892<br>0.2821<br>0.4280<br>0.3826<br>0.3826<br>0.5803<br>0.4832<br>0.4832<br>0.4832<br>0.4832<br>0.4832   | 0.1532<br>0.1539<br>0.1539<br>0.2892<br>0.2892<br>0.2821<br>0.4280<br>0.4280<br>0.4832<br>0.4832<br>0.4146<br>0.4146   | 0.1532<br>0.1539<br>0.2892<br>0.2892<br>0.2821<br>0.4280<br>0.3826<br>0.3826<br>0.5803<br>0.4832<br>0.4146<br>0.4146<br>0.4146<br>0.4146   
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& \\ & & \\$   | $\begin{array}{c} & & & \\ & & & & \\ & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & & \\ & & & & & \\ & & & & \\ & & & & & \\ & & & & & \\ & & & & \\$  | $\begin{array}{c} 0.1532\\ 0.1539\\ 0.2892\\ 0.2892\\ 0.2892\\ 0.2892\\ 0.3826\\ 0.3826\\ 0.3826\\ 0.3826\\ 0.3826\\ 0.3826\\ 0.3826\\ 0.3826\\ 0.3826\\ 0.3821\\ 0.2793\\ 0.2770\\ 0.2793\\ 0.2773\\ 0.2793\\ 0.2773\\ 0.2793\\ 0.2773\\ 0.2793\\ 0.2773\\$  | $\begin{array}{c} 0.1532\\ 0.1539\\ 0.2892\\ 0.2892\\ 0.2892\\ 0.2892\\ 0.2892\\ 0.2826\\ 0.4280\\ 0.3826\\ 0.3826\\ 0.3826\\ 0.3826\\ 0.3826\\ 0.3826\\ 0.3821\\ 0.2773\\
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|             |                  |                                    |          |                      |          | 2.266     |                |                              | 1.905                |          |   |   |   | 3.091   |   | 3.091<br>2.849<br>2.507  | 3.091<br>2.849<br>2.507<br>1.476  |  
   |   | 3.091<br>2.849<br>2.507<br>1.476<br>1.528<br>1.413<br>1.616   | 3.091<br>2.507<br>2.507<br>1.476<br>1.476<br>1.413<br>1.413<br>1.616<br>1.616  | 3.091<br>2.849<br>2.507<br>1.476<br>1.528<br>1.413<br>1.616<br>1.516<br>1.392   | 3.091<br>2.849<br>2.507<br>1.476<br>1.528<br>1.413<br>1.616<br>1.392<br>1.556  
   | 3.091<br>2.849<br>2.507<br>1.476<br>1.476<br>1.528<br>1.616<br>1.392<br>1.556  | 3.091<br>2.849<br>2.507<br>1.476<br>1.476<br>1.476<br>1.528<br>1.616<br>1.392<br>1.556<br>1.556<br>1.580   | 3.091<br>2.849<br>2.507<br>1.476<br>1.476<br>1.476<br>1.528<br>1.616<br>1.528<br>1.616<br>1.556<br>1.556<br>1.556  | 3.091<br>2.849<br>2.507<br>1.476<br>1.476<br>1.413<br>1.616<br>1.528<br>1.616<br>1.556<br>1.556<br>1.556<br>1.580<br>1.580   
   | 3.091<br>2.507<br>2.507<br>2.549<br>1.476<br>1.476<br>1.528<br>1.413<br>1.616<br>1.528<br>1.556<br>1.556<br>1.580<br>1.580<br>1.580   | 3.091<br>2.507<br>2.507<br>2.516<br>1.476<br>1.476<br>1.528<br>1.413<br>1.616<br>1.528<br>1.556<br>1.556<br>1.580<br>1.580<br>1.580<br>1.580<br>1.580  | $\begin{array}{c} 3.091\\ 2.507\\ 2.507\\ 2.507\\ 1.476\\ 1.528\\ 1.413\\ 1.616\\ 1.580\\ 1.$   | $\begin{array}{c} 3.091\\ 2.507\\ 2.507\\ 2.507\\ 1.476\\ 1.476\\ 1.528\\ 1.413\\ 1.616\\
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  | $\begin{array}{c} 3.091\\ 2.507\\ 2.507\\ 2.507\\ 2.507\\ 1.476\\ 1.528\\ 1.413\\ 1.616\\ 1.580\\ 1.580\\ 1.580\\ 1.580\\ 1.580\\ 1.580\\ 1.580\\ 1.580\\ 1.580\\ 1.592\\ 1.$   | $\begin{array}{c} & - & - \\ & 3.091 \\ & 2.849 \\ & 2.849 \\ & 2.849 \\ & 1.476 \\ & 1.528 \\ & 1.616 \\ & -$   | $\begin{array}{c} 3.091\\ 2.849\\ 2.507\\ 2.507\\ 2.849\\ 1.476\\ 1.528\\ 1.413\\ 1.616\\ 1.580\\ 1.580\\ 1.580\\ 1.580\\ 1.580\\ 1.580\\ 1.580\\ 1.580\\ 1.592\\ 1.592\\ 1.592\\ 1.592\\ 1.592\\ 1.592\\ 1.592\\ 1.592\\ 1.592\\ 1.592\\ 1.592\\ 1.592\\ 1.592\\ 1.592\\ 1.592\\ 1.521\\ 1.592\\ 1.521\\ 1.51\\ 1.51\\ 1.522\\
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   | $\begin{array}{c} 3.091\\ 2.507\\ 2.507\\ 2.507\\ 2.507\\ 2.507\\ 1.476\\ 1.528\\ 1.416\\ 1.580\\ 1.580\\ 1.580\\ 1.580\\ 1.580\\ 1.580\\ 1.580\\ 1.580\\ 1.592\\ 1.$   |
|             |                  | 321                                | 321      | 369<br>374           | 299      | 262       | 341            | 100                          | 188                  | 356      | 303                                     | 380   | 251   | 100   | 320<br>320  | 320<br>502   | 320<br>502<br>208   | 502<br>502<br>208<br>181   
   | 204<br>320<br>502<br>208<br>181<br>295  | 204<br>320<br>208<br>208<br>181<br>312<br>312   | 502<br>502<br>208<br>181<br>174<br>174<br>174  | 502<br>502<br>1208<br>181<br>174<br>187<br>487  | 502<br>502<br>1208<br>1312<br>1174<br>487<br>487<br>487<br>406   
   | 502<br>502<br>1208<br>181<br>172<br>174<br>487<br>487<br>487<br>485  | 202<br>502<br>502<br>208<br>181<br>174<br>187<br>487<br>487<br>485<br>411  | 202<br>502<br>502<br>208<br>181<br>174<br>487<br>487<br>487<br>487<br>487<br>487<br>487<br>423   | 202<br>502<br>502<br>208<br>181<br>174<br>487<br>487<br>487<br>487<br>411<br>423<br>419  
   | 201<br>502<br>502<br>502<br>181<br>181<br>181<br>181<br>487<br>487<br>487<br>411<br>411<br>411<br>335<br>335<br>375<br>375  | 201<br>202<br>502<br>502<br>181<br>181<br>181<br>187<br>487<br>487<br>487<br>411<br>411<br>411<br>433<br>335<br>335<br>332<br>434  | 202<br>502<br>502<br>502<br>181<br>181<br>181<br>181<br>487<br>487<br>487<br>487<br>411<br>411<br>411<br>411<br>411<br>110  |
200<br>500<br>502<br>502<br>508<br>181<br>181<br>181<br>181<br>181<br>487<br>487<br>487<br>487<br>487<br>487<br>487<br>487   | 227<br>502<br>502<br>502<br>508<br>181<br>174<br>487<br>487<br>487<br>487<br>487<br>411<br>110<br>110<br>139<br>527<br>527<br>527<br>527<br>527<br>527<br>527<br>527<br>527<br>527  | 200<br>502<br>502<br>502<br>181<br>174<br>487<br>487<br>487<br>487<br>487<br>487<br>487<br>487<br>487<br>4  
   | 200<br>500<br>502<br>502<br>508<br>181<br>174<br>487<br>487<br>487<br>487<br>487<br>487<br>487<br>411<br>110<br>110<br>139<br>227<br>2231<br>2231<br>2231  | 202<br>502<br>502<br>502<br>181<br>174<br>487<br>487<br>487<br>487<br>487<br>411<br>110<br>139<br>335<br>533<br>372<br>227<br>227<br>223<br>139<br>224<br>224  | 200<br>201<br>202<br>202<br>208<br>208<br>181<br>181<br>208<br>487<br>487<br>487<br>487<br>487<br>487<br>487<br>48  | 200<br>201<br>202<br>202<br>208<br>208<br>208<br>208<br>487<br>487<br>487<br>487<br>487<br>487<br>487<br>48   
   | 253<br>253<br>200<br>200<br>201<br>201<br>202<br>202<br>203<br>203<br>203<br>203<br>203<br>203<br>203<br>203   | 202<br>202<br>208<br>208<br>208<br>208<br>208<br>411<br>411<br>412<br>413<br>411<br>413<br>413<br>413<br>413<br>413<br>413<br>413<br>413  |
202<br>202<br>202<br>208<br>208<br>181<br>174<br>487<br>487<br>487<br>487<br>487<br>411<br>130<br>133<br>224<br>130<br>130<br>132<br>224<br>130<br>130<br>224<br>224<br>130<br>2253<br>233<br>233<br>233<br>233<br>233<br>233<br>233<br>233<br>23  | 202<br>502<br>502<br>502<br>503<br>181<br>174<br>487<br>487<br>487<br>487<br>487<br>487<br>487<br>411<br>110<br>1110<br>1110<br>1110<br>222<br>223<br>224<br>224<br>2231<br>224<br>2231<br>2231<br>2231   
  | 200<br>201<br>201<br>202<br>203<br>208<br>208<br>208<br>208<br>208<br>208<br>208<br>208   | 200<br>201<br>202<br>208<br>208<br>208<br>208<br>208<br>487<br>487<br>487<br>487<br>487<br>487<br>487<br>48  | 200<br>201<br>202<br>208<br>208<br>208<br>208<br>208<br>208<br>208  
   | 200<br>201<br>201<br>202<br>203<br>208<br>208<br>208<br>208<br>208<br>208<br>208<br>208   | 200<br>201<br>201<br>201<br>201<br>201<br>201<br>201<br>201<br>201  
   |
|             |                  | 51.49°W)<br>111                    | 139      | 110<br>103           | 139      | 104       | 101            | (M_04.1CI                    | 2/0<br>120           | 94.8     | 49.8                                    | 113   | 90.8  |   | 67.5<br>101   | 67.5<br>191<br>-151.04° W  | 67.5<br>191<br>-151.04° W_<br>137   | 67.5<br>191<br>- <i>151.04° W</i><br>137<br>108  
   | 67.5<br>191<br>- <i>151.04° W</i><br>1137<br>108<br>166   | 67.5<br>191<br>- <i>151.04° W</i> ,<br>137<br>108<br>166<br>228   | 67.5<br>191<br>137<br>137<br>137<br>108<br>166<br>153<br>153   | 67.5<br>191<br>-151.04° W,<br>137<br>108<br>166<br>153<br>153<br>134<br>108   | 67.5<br>191<br>-151.04° W,<br>137<br>108<br>166<br>153<br>153<br>153<br>108<br>108   
   | 67.5<br>191<br>131<br>137<br>166<br>166<br>168<br>153<br>153<br>153<br>153<br>153<br>153<br>108<br>108<br>108<br>97.1  | 67.5<br>191<br>131<br>137<br>116<br>166<br>168<br>153<br>153<br>153<br>153<br>153<br>153<br>153<br>153<br>153<br>153   | 67.5<br>191<br>151.04° W,<br>137<br>108<br>166<br>1228<br>153<br>134<br>108<br>108<br>97.1<br>97.1<br>92.7   | 67.5<br>191<br>151.04° W,<br>137<br>108<br>166<br>134<br>1134<br>108<br>97.1<br>97.1<br>92.7<br>92.7   
   | 67.5<br>191<br>131<br>137<br>166<br>166<br>153<br>153<br>153<br>168<br>108<br>97.1<br>97.1<br>97.1<br>124<br>124<br>94.7<br>94.7<br>94.7<br>94.7  | 67.5<br>191<br>137<br>137<br>137<br>138<br>158<br>158<br>158<br>108<br>97.1<br>97.1<br>97.1<br>97.1<br>108<br>97.1<br>97.1<br>118<br>97.1<br>118   | 67.5<br>191<br>137<br>137<br>137<br>138<br>158<br>158<br>158<br>108<br>108<br>108<br>97.1<br>97.1<br>97.1<br>108<br>97.1<br>118<br>97.1<br>118<br>97.1<br>124<br>97.1<br>124<br>97.1<br>128<br>97.1<br>128<br>97.1<br>128<br>128<br>128<br>128<br>128<br>128<br>128<br>128<br>128<br>12   |
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  | ( <i>6.81°S</i> , <i>16.81°S</i> ,   | ( <i>b</i> , <i>b</i> , <i>c</i>  | ( <i>b</i> , <i>b</i> , <i>c</i>  
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| mple ID     |                  | <i>thaa (16.58–16.</i><br>A13-01-1 | A13-02-1 | A13-03-1<br>A13-06-1 | A13-07-1 | A13-10-1  | A13-11-1       | aiatea (10.80–1<br>Troz 01 1 | T03-02-1<br>T03-02-1 | T03-03-2 | T03-04-2                                | T03-05-1  | T03-06-2  | T03-07-1  | A 01 15 1   | A01-15-1<br>hahine (16.74–   | A01-15-1<br>luahine (16.74–<br>IH05-01-2w   | A01-15-1<br><sup>t</sup> uahine (16.74<br>IH05-01-2w<br>IH05-02-2  
   | A01-15-1<br><sup>t</sup> uahine (16.74<br>H05-01-2w<br>H05-02-2<br>H05-03-2w  | A01-15-1<br>tuahine (16.74<br>H05-01-2w<br>H05-02-2<br>H05-03-2w<br>H05-05-2w   | A01-15-1<br>' <i>uahine (16.74</i><br>H05-01-2w<br>H05-02-2<br>H05-03-2w<br>H05-05-2w<br>H05-06-2  | A01-15-1<br>'udhine (16.74<br>H05-01-2w<br>H05-02-2<br>H05-03-2w<br>H05-06-2<br>H05-06-2<br>H06-01-2<br>H06-01-2  | A01-15-1<br>uahine (16.74-,<br>H05-01-2w<br>H05-02-2<br>H05-03-2w<br>H05-05-2w<br>H05-06-2<br>H06-01-2<br>H06-01-2<br>H06-02-2   
   | A01-15-1<br>uahine (16.74-,<br>H05-01-2w<br>H05-01-2w<br>H05-03-2w<br>H05-05-2w<br>H05-05-2<br>H06-01-2<br>H06-01-2<br>H06-01-2<br>H06-03-2  | A01-15-1<br>uahine (16.74-,<br>H05-01-2w<br>H05-02-2<br>H05-03-2w<br>H05-05-2<br>H05-07-2<br>H06-01-2<br>H06-01-2<br>H06-01-2<br>H06-03-2<br>H06-04-1  | A01-15-1<br>uahine (16.74-,<br>H05-01-2w<br>H05-01-2w<br>H05-05-2<br>H05-05-2<br>H05-05-2<br>H05-01-2<br>H06-01-2<br>H06-01-2<br>H06-04-1<br>H06-04-1<br>H06-04-2<br>H06-04-2  | A01-15-1<br>uahine (16.74-,<br>H05-01-2w<br>H05-01-2w<br>H05-05-2<br>H05-05-2<br>H05-05-2<br>H05-02-2<br>H06-01-2<br>H06-01-2<br>H06-04-1<br>H06-03-2<br>H06-05-2<br>H06-05-2<br>H06-05-2  
   | A01-15-1<br>uahine (16.74-,<br>H05-01-2w<br>H05-02-2<br>H05-03-2w<br>H05-05-22w<br>H05-05-2<br>H06-01-2<br>H06-01-2<br>H06-04-1<br>H06-04-2<br>H06-06-3<br>H06-06-3<br>H06-06-3   | A01-15-1<br>uahine (16, 74-,<br>1405-01-2w<br>1405-02-2<br>1405-02-2<br>1405-05-2w<br>1405-05-2<br>1406-01-2<br>1406-01-2<br>1406-04-1<br>1406-04-2<br>1406-05-2<br>1406-05-2<br>1406-05-2<br>1406-05-2<br>1406-05-2   | A01-15-1<br>uahine (16, 74-,<br>H05-01-2w<br>H05-02-2<br>H05-02-2<br>H05-05-22w<br>H05-05-2<br>H06-01-2<br>H06-01-2<br>H06-04-1<br>H06-04-2<br>H06-04-2<br>H06-06-3<br>H06-06-3<br>H06-06-3<br>H06-07-2<br>H06-07-2<br>H06-07-2   | A01-15-1<br>uahine (16,
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   | A01-15-1<br>uahine (16, 74-,<br>105-01-2w<br>1105-02-2<br>1105-02-2<br>1105-03-22w<br>1105-05-22w<br>1106-03-2<br>1106-03-2<br>1106-04-1<br>1106-04-2<br>1106-04-2<br>1106-05-2<br>1106-05-2<br>1106-05-2<br>1106-05-2<br>1107-07-1w<br>1108-01-2<br>1108-02-1<br>1108-02-2<br>1108-02-2<br>1108-02-2<br>1108-02-2<br>1108-02-2<br>1108-02-2<br>1108-02-2<br>1108-02-2<br>1108-02-2<br>1108-02-2   | A01-15-1<br>uahine (16, 74-,<br>105-01-2w<br>1105-02-2<br>1105-02-2<br>1105-03-22w<br>1105-05-22w<br>1106-01-2<br>1106-01-2<br>1106-01-2<br>1106-01-2<br>1106-05-2<br>1106-05-2<br>1106-05-2<br>1106-05-2<br>1106-05-2<br>1107-01-1w<br>1108-01-2<br>1108-01-2<br>1108-02-2<br>1108-02-1<br>1108-02-1<br>1108-02-2<br>1108-02-2<br>1108-02-2<br>1108-02-2<br>1108-02-2<br>1108-02-2<br>1108-02-2<br>1108-02-2<br>1108-02-2<br>1108-02-2<br>1108-02-2<br>1108-02-2<br>1108-02-2<br>1108-02-2<br>1108-02-2<br>1108-02-1  | A01-15-1<br>uahine (16, 74-,<br>105-01-2w<br>105-02-2<br>105-05-22w<br>105-05-22w<br>106-01-2<br>106-01-2<br>106-01-2<br>106-02-2<br>106-04-1<br>106-04-2<br>1106-05-2<br>1106-05-2<br>1106-05-2<br>1106-05-2<br>1106-05-2<br>1108-01-2<br>1108-01-2<br>1108-01-2<br>1108-01-2<br>1108-01-2<br>1108-01-2<br>1108-01-2<br>1108-01-2<br>1108-01-2<br>1108-01-2<br>1108-01-2<br>1108-01-2<br>1108-01-2   | A01-15-1<br>utabine (16, 74-,<br>105-01-2w<br>105-02-2<br>105-05-2w<br>105-05-2w<br>105-05-2w<br>106-01-2<br>106-01-2<br>106-01-2<br>106-02-2<br>106-04-1<br>106-04-2<br>106-04-2<br>106-05-2<br>106-05-2<br>106-05-2<br>106-05-2<br>106-05-2<br>106-05-2<br>108-04-1<br>108-04-1<br>108-04-2<br>108-04-2<br>108-04-2<br>108-04-2   
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coefficients of the intest NKM-1KM1 <sup>-1</sup> and 1KM1-1KM2 <sup>-2</sup> segments; $f_N$ , $f_T$ , NKM and 1KM1 fractions of the intest NKM-1KM1 <sup>+2</sup> and 1KM1-1KM2 <sup>-2</sup> segments; $F_L$ , iaboratory induced DC
and TRM2; F, calculated palaeointensity; $\Delta AIC$ , AIC difference between linear and quadratic fit (AIC1–AIC2). Note that palaeointensities from specimens with suffix, w' are calculated with cor
changes.
Not adopted for the calculation of the flow average (because of the possible low temperature oxidation suggested from the $M_{s-T}$ curve of Type E).
<sup>2</sup> Not adopted for the calculation of the flow average (because of the curved NRM-TRM1* diagram).

Table 1. ( $C_{\ell}$	ontinuec	<i>d.</i> )																		
Sample ID	НТ	LT	NRM <sub>0</sub>	$ARMO_0$	$B_{ m rc}/B_{ m c}$	$M_{ m rs}/M_{ m s}$	LTD			First heating				S	econd heatir	lg		$F_{\mathrm{L}}$	Ľ.	∆AIC
							(per cent)	$H_{\rm L}$	Slope $_{\rm A}$	Slope $_{\rm N}$	$f_{\mathrm{N}}$	$r_{\rm N}$	$H_{\mathrm{L}}$	Slope $_{\rm A}$	Slope $_{\rm T}$	$f_{\mathrm{T}}$	$r_{\mathrm{T}}$	$(\mu T)$	$(\mu T)$	
HH13-07-1			290	440	1.553	0.3622	7.4	35	0.604	0.167	0.136	0.985	35	0.632	1.91	0.427	0.993	50.0		
HH14-06-1	D		127	135	1.557	0.3585	5.7	15	0.301	0.132	0.107	0.984	30	0.884	2.23	0.708	0.995	40.0		
HH15-02-1			302	495	1.939	0.1746	16.7	20	0.410	0.140	0.140	0.99I	15	0.920	2.00	0.899	0.999	40.0		
HH15-03-1			341	451	1.878	0.1696	15.3	10	0.379	0.227	0.194	0.955	20	0.876	1.91	0.720	0.998	40.0		
Tahiti (17.52–	17.78°S,	149.17-1	(49.59° W)																	
PU04-01-2			155	312	1.892	0.2365	13.0	10	0.459	1.09	0.575	0.997	5	0.898	0.998	0.947	0.999	20.0	21.8	0.1
PU04-02-1	ц	c	195	335	1.845	0.2200	9.9	15	0.359	0.597	0.400	0.997	5	0.946	0.972	0.955	0.999	40.0	23.9	3.6
PU04-03-2			165	320	1.747	0.2586	9.9	10	0.495	1.11	0.598	0.995	5	0.911	1.02	0.938	0.999	20.0	22.2	3.3
PU04-06-1			162	245	1.848	0.2291	31.5	10	0.453	0.557	0.587	0.996	5	0.891	1.02	0.952	0.999	40.0	22.3	11.6
PU04-11-1			388	224			9.9	50	1.47	2.48	0.257	0.991	0	0.925	1.39	1.00	0.999	40.0		
PU04-12-1			175	351	1.821	0.2331	11.5	10	0.460	1.10	0.573	0.997	5	0.922	0.977	0.944	0.998	20.0	22.0	-0.5
PU05-01-2			135	483	1.639	0.2708	9.1	15	0.187	0.634	0.342	0.997	0	0.985	1.03	1.00	0.999	20.0	12.7	5.8
PU05-02-1	ц	J	116	324	1.904	0.2305	16.0	10	0.451	0.349	0.416	0.995	5	0.859	1.04	0.915	0.999	40.0	14.0	4.2
PU05-03-2			142	323	2.031	0.2334	13.0	10	0.538	0.865	0.411	0.998	20	0.827	1.02	0.697	0.998	20.0	17.3	13.1
PU05-04-1			130	316	1.913	0.2260	15.3	10	0.425	0.389	0.410	0.995	5	0.852	1.00	0.908	0.999	40.0	15.6	4.8
PU05-05-2			190	432			14.5	15	0.152	1.22	0.199	0.995	0	0.969	1.11	1.00	0.995	10.0		
PU05-11-1			172	346			16.7	10	0.663	0.574	0.435	0.996	15	0.913	1.21	0.572	0.998	40.0		
PU05-12-1			144	312	2.141	0.2006	11.5	10	0.282	0.799	0.292	0.995	5	0.859	0.985	0.897	0.996	20.0	16.0	10.2
PU06-01-2			655	271			3.8	50	1.36	4.32	0.316	0.979	0	1.00	1.01	1.00	1.00	20.0		
PU06-04-1	A	a	536	244	1.860	0.3397	-3.1	55	1.09	2.57	0.429	0.936	0	1.03	0.973	1.00	1.00	40.0		
PU06-05-1			794	349			3.8	55	1.08	1.88	0.226	0.978	0	1.03	1.02	1.00	1.00	40.0		
PU06-11-1			857	342			5.7	50	1.18	5.27	0.317	0.988	0	1.04	1.00	1.00	1.00	20.0		
PU06-21-2			1310	397			4.8	25	1.07	3.83	0.879	0.991	0	1.02	1.05	1.00	0.999	20.0		
PU06-23-2			1450	415			5.7	25	1.04	4.04	0.870	0.994	0	1.04	0.987	1.00	1.00	20.0		
PU06-31-2	A	а	1440	450	1.659	0.3973	-7.5	40	0.959	2.22	0.682	0.972	0	1.02	1.02	1.00	1.00	40.0		
TR02-01-2			76.4	412			21.9	10	0.828	0.432	0.996	0.979	5	0.942	1.08	0.883	0.999	20.0		
TR02-02-1			103	397	2.676	0.2039	18.7	10	0.793	0.502	0.832	0.997	0	1.01	1.00	1.00	0.999	20.0	10.0	0.6
TR02-03-2	в		6.09	402	3.773	0.2018	24.8	15	0.976	0.790	0.967	0.995	0	0.951	1.02	1.00	0.998	10.0	7.90	-1.0
TR02-04-1			100	381	2.586	0.2270	22.5	15	0.979	0.483	0.823	0.995	5	0.947	1.05	0.894	0.999	20.0	9.66	1.0
TR02-06-1			98.1	398	2.586	0.2270	18.0	15	0.904	0.461	0.731	0.996	5	0.946	0.984	0.884	0.998	20.0	9.22	16.3
TH02-01-2			310	679			-17.4	15	0.473	0.870	0.583	0.998	10	0.963	1.09	0.931	0.999	20.0		
TH02-03-2			326	765	2.184	0.1648	-2.9	15	0.494	1.30	0.688	0.998	10	0.908	1.04	0.943	0.999	20.0	26.0	5.1
TH02-04-1	V		356	742	2.115	0.1759	-15.6	15	0.541	0.736	0.722	0.997	10	1.00	0.958	0.946	1.00	40.0	29.4	-0.4
TH02-13-1			217	598			19.4	25	0.545	0.531	0.396	0.995	10	0.942	1.07	0.951	1.00	20.0		
TH03-03-2			36.3	425	2.192	0.1844	16.7	10	0.668	0.191	0.961	0.995	5	1.01	1.04	0.989	0.998	20.0	3.82	1.0
TH03-09-1			32.9	245	1.946	0.1918	18.7	20	1.03	0.261	0.647	0.995	0	0.985	1.01	1.00	1.00	20.0	5.22	13.1
TH03-12-1	A		12.9	322	2.063	0.1881	22.5	5	0.772	0.054	2.10	0.943	0	1.03	0.986	1.00	0.999	40.0		
TH03-16-2			28.8	213	2.291	0.1578	22.5	20	1.04	0.254	0.745	0.995	0	1.01	0.978	1.00	1.00	20.0	5.08	7.0
TH04-03-1			230	839			2.0	10	0.330	0.481	0.489	0.98I	30	0.974	1.03	0.610	0.998	20.0		
TH04-04-1			229	673			18.0	10	0.370	0.543	0.575	0.983	30	0.986	1.05	0.655	0.998	20.0		
TH04-13-1	в		194	638	2.030	0.3313	15.3	10	0.488	0.231	0.798	0.995	20	1.00	0.983	0.954	0.998	40.0	9.24	25.5
HT. LT. class:	fication	is of the t	hermomag	netic and l	ow-temper	ature cvcling	curves: NRI	M <sub>0</sub> . ARI	M0 <sub>0</sub> , initial	NRM and	ARM0 int	ensity afte	r LTD (	$10^{-5} \text{ A} \text{ m}^2$	$kg^{-1}$ ); $B_{rc}$	$ B_{\rm c},M_{ m rs} $	/Ms. core	-average	l ratios of	
remanent coe	rcivity t	to coerciv	ity and sat	uration me	enetization	to remanen	t saturation n	nagnetiz	ation: LTD.	LT demagr	etized fra	ction of A	RM0 (n	er cent): H	r. the lowe	st coercivi	ity force to	uken for t	ne linear	
segments: Slo	merisle	one of Al	RM snectra	$h(h_{T}) h$	ح efore and a	fter laborato	rv heating: S	lonen. S	loner. slon	ہ of the line	ar segmer	its in the	NRM-T	RM1* and	TRM1-TR	M2* diagr	ams: r M.	rr. corre	ation	
coefficients o	f the lin	ear NRM	TRM1*	and TR MI	_TRM7* s	ements. f.	fr NRM	TR N	Al fractions	of the line	r NR M-T	RM1* an	d TRM	_TRM7*	eaments. F	r lahorat	orthri vro	ad DC fie	ld for TR	IW
CONTINUINT	luni viti I	nurri uda		V ULV V	o 7IANTI_	cguruus, j N	1. J. I, J. WINT (			OI ULUN NIO	- 141-414 11	INIVI IIIII	TANT D	- 7IMMIT_	veguvuls, 1	L, tauut ui ' ano ao'	white the second		and parties	TIAD
and TKIMZ; r	, calcui	lated paia	contensity	'; ΔΑΙ <b></b> Ο, Α	ALC differen	nce between	linear and qu	adratic I	it (AlUI–A	JCZ). Note	that palae	ointensiu	es trom	specimens	with sumx	w are ca	lculated w	ith correct	tions for	mass

Table 2. $Ex_{F}$	erimen	ital resu	lts from the	EHD-DHI	Shaw meth	nod for the la	va sequences													
Sample ID	ΗT	LT	$NRM_0$	$ARM0_0$	$B_{ m rc}/B_{ m c}$	$M_{ m rs}/M_{ m s}$	LTD			First heating				S	econd heati	1g		$F_{\rm L}$	ц	ΔAIC
							(per cent)	$H_{\mathrm{L}}$	$Slope_A$	Slope <sub>N</sub>	$f_{\rm N}$	$r_{\rm N}$	$H_{\mathrm{L}}$	$Slope_A$	$Slope_{T}$	$f_{\mathrm{T}}$	$r_{\mathrm{T}}$	$(\mu T)$	$(\mu T)$	
Maupiti seque	nce A (1	6.44°S,	152.25°W)																	
MP13-02-1			712	697	1.620	0.2870	5.7	S	0.752	1.20	0.417	0.995	10	0.906	0.953	0.851	0.999	20.0	24.0	69.5
MP13-03-1			397	470			8.3	15	0.389	2.55	0.349	0.995	10	1.04	0.946	0.935	0.996	10.0		
MP13-04-1			330	436			10.7	10	0.368	1.18	0.466	0.997	0	1.07	0.937	1.00	0.996	20.0		
MP13-05-2			267	340			5.7	10	1.04	1.34	0.970	0.989	0	1.05	0.882	1.00	1.00	20.0		
MP13-06-2			452	577			8.3	10	0.543	1.18	0.442	0.998	20	1.01	0.89I	0.767	0.999	20.0		
MP13-07-1	C	с	392	524	1.601	0.2936	9.6	10	0.482	1.33	0.432	0.995	35	0.751	1.01	0.481	0.995	20.0	26.6	10.1
MP12-02-1			243	331			6.5	50	0.737	0.530	0.208	0.985	5	0.838	0.916	0.962	0.997	20.0		
MP12-03-1			265	386	1.761	0.3443	8.3	35	0.621	1.28	0.346	0.995	0	0.904	0.981	1.00	0.999	10.0	$12.8^{\rm a}$	14.7
MP12-04-1			299	391		I	3.8	15	0.703	1.03	0.639	0.998	10	0.886	0.926	0.936	0.998	20.0		
MP12-05-2			230	463	1.510	0.5070	2.0	10	0.427	0.712	0.753	0.999	0	1.03	1.05	1.000	0.999	20.0	$14.2^{\mathrm{a}}$	-0.9
MP12-06-2			231	448	1.372	0.5150	5.7	20	0.319	0.689	0.624	0.998	0	1.02	1.04	1.00	0.999	20.0	$13.8^{\rm a}$	-0.6
MP12-07-1	Ш	q	452	799	1.357	0.5890	0.0	10	0.674	0.932	0.809	0.996	0	1.03	0.997	1.00	0.999	20.0	$I8.6^{a}$	0.2
MP11-02-1			618	530			2.9	20	0.971	1.28	0.672	0.998	0	0.980	1.07	1.00	1.00	20.0		
MP11-06-1			540	549	1.456	0.4238	9.1	15	0.713	1.24	0.835	0.999	0	0.999	1.05	1.00	1.00	20.0	24.8	16.7
MP10-05-1			497	918	1.864	0.2817	2.9	0	1.11	0.948	1.00	1.00	0	1.03	1.02	1.00	1.00	20.0	19.0	7.4
MP10-07-1			305	353		I	5.7	20	0.481	1.17	0.704	0.998	0	0.980	1.07	1.00	1.00	20.0		
MP09-03-1			518	436			10.7	15	0.694	1.48	0.864	0.980	0	1.02	0.972	1.00	1.00	20.0		
MP09-07-1			365	411		I	9.1	15	0.885	1.33	0.793	0.991	0	0.986	0.973	1.00	1.00	20.0		
MP08-03-1			311	398			7.4	15	0.883	1.27	0.703	0.991	0	1.01	0.992	1.00	1.00	20.0		
MP08-07-1			270	377			11.5	20	0.846	1.42	0.636	0.994	0	0.998	1.00	1.00	1.00	20.0		
MP07-03-1			475	480			5.7	15	1.02	1.55	0.835	0.995	0	1.02	0.989	1.00	1.00	20.0	31.0	34.0
MP07-07-1			296	355	2.080	0.1797	14.5	20	1.03	1.75	0.722	0.995	0	1.01	0.977	1.00	1.00	20.0	35.0	53.5
MP06-05-1			388	386	1.986	0.2699	8.3	25	0.973	1.88	0.568	0.995	0	0.997	1.00	1.00	1.00	20.0	37.6	42.6
MP06-07-1			342	385			6.5	20	1.07	1.63	0.612	0.996	0	1.01	0.976	1.00	1.00	20.0	32.6	50.7
MP05-05-1			246	342	2.195	0.1839	12.3	25	0.841	1.67	0.581	0.995	0	0.998	0.995	1.00	1.00	20.0	33.4	45.1
MP05-07-1			316	420			2.9	20	0.940	1.52	0.645	0.997	0	1.01	0.960	1.00	1.00	20.0	30.4	16.8
MP04-05-1			287	263			13.8	15	0.764	1.60	0.664	0.988	0	0.987	1.06	1.00	1.00	20.0		
MP04-08-1			360	369	1.563	0.2697	8.3	15	0.653	1.36	0.621	0.999	0	0.969	1.05	1.00	1.00	20.0	27.2	-0.6
MP03-03-1			579	553	1.762	0.2651	5.7	25	0.847	1.61	0.593	0.995	0	1.00	0.985	1.00	1.00	20.0	32.2	18.9
MP03-07-1			371	336			9.1	35	0.795	1.98	0.339	0.994	0	1.00	1.04	1.00	1.00	20.0		
MP02-02-1			339	416			7.4	15	0.704	1.19	0.883	0.992	0	1.00	1.05	1.00	0.999	20.0		
MP02-03-1	В	а	353	461	1.555	0.4153	4.8	15	0.783	2.22	0.888	0.995	0	1.02	1.05	1.00	0.999	10.0	22.2	9.1
MP02-04-2			339	449	1.555	0.4200	5.7	20	0.814	0.989	0.813	0.995	0	1.02	1.04	1.00	0.999	20.0	19.8	35.1
MP02-06-1			366	455	1.491	0.4371	5.7	15	0.703	1.19	0.892	0.995	0	1.05	1.01	1.00	766.0	20.0	23.8	-1.7
MP02-07-1			320	348			3.8	25	0.432	1.89	0.667	0.996	0	1.09	0.947	1.00	0.996	20.0		
MP02-08-1			308	337			4.8	30	0.359	1.97	0.546	0.994	0	1.03	1.03	1.00	0.980	20.0		

Table 2. (Con.	tinued.																			
Sample ID	ΗТ	LT	$NRM_0$	$ARM0_0$	$B_{ m rc}/B_{ m c}$	$M_{ m rs}/M_{ m s}$	LTD		Π	First heating				Š	scond heatin	50		$F_{\rm L}$	F	AAIC
							(per cent)	$H_{\rm L}$	$Slope_A$	Slope <sub>N</sub>	$f_{\rm N}$	$r_{\rm N}$	$H_{\mathrm{L}}$	$Slope_A$	$Slope_{T}$	$f_{\mathrm{T}}$	$r_{\mathrm{T}}$	$(\mu T)$	$(\mu T)$	
Borabora Seque	nce A (1	16.54°S,	151.73°W)	660	1 600	10100	11 6	ų	0000	0 5 10	7770	0.005	30	2000	0.050	0.400	200.0	0.00	0.11	100
BR07-01-1 BR07-02-1			219	515	700.1		16.0	01	0.200	1.89	0.220	0.982	c) c	0.942	767.0	1.00	0.990	10.0	0.11	1.02
BR07-05-1	V		156	288	2.501	0.1520	12.3	20	0.696	1.18	0.567	0.998	0	1.01	0.985	1.00	0.999	20.0	23.6	6.3
BR07-06-1			284	427	2.146	0.2407	14.5	15	0.553	3.55	0.678	0.997	2	0.974	0.979	0.962	0.998	10.0	35.5	24.3
BR04-01-2			283	364	2.109	0.2006	16.0	10	0.757	0.966	0.777	0.995	0	0.962	0.973	1.00	1.00	30.0	29.0	28.8
BR04-02-1	A	в	269	400	2.113	0.1536	17.4	15	0.658	1.29	0.671	0.996	5	0.913	1.04	0.949	0.999	20.0	25.8	6.4
BR04-03-2			294	547	1.905	0.3087	15.3	10	0.564	0.739	0.620	0.998	5	0.879	0.989	0.921	0.999	30.0	22.2	30.4
BR04-04-1w			246	426			16.0	10	0.524	0.966	0.539	0.999	5	0.848	0.922	0.952	0.997	20.0		
BR04-06-2			337	534			9.1	15	0.573	1.29	0.640	0.997	0	0.939	1.16	1.00	0.999	20.0		
BR04-07-1			384	550	1.713	0.3425	13.0	10	0.660	1.460	0.785	0.996	0	0.988	0.994	1.00	1.00	20.0	29.2	-1.9
Borabora sequer	rce B (1	16.47°S,	151.76°W)																	
BR15-01-2			65.1	267	2.496	0.1304	24.8	20	0.716	0.791	0.420	0.996	0	0.980	0.950	1.00	1.00	20.0	15.8	0.9
BR15-02-1			66.7	286	2.698	0.1250	23.7	20	0.737	0.699	0.467	0.995	0	0.925	0.984	1.00	0.999	20.0	14.0	11.4
BR15-03-1			70.7	280	2.620	0.1590	21.3	20	0.729	1.19	0.392	0.995	0	0.915	1.00	1.00	0.998	10.0	11.9	-0.9
BR15-05-1	В	а	75.1	223	2.346	0.1645	22.5	20	0.700	0.730	0.419	0.995	0	0.973	1.01	1.00	1.00	20.0	14.6	7.8
BR15-06-2			6.69	219	2.448	0.1484	21.3	15	0.654	1.45	0.519	0.995	0	0.924	1.01	1.00	0.998	10.0	14.5	32.2
BR15-07-1			82.4	211	2.330	0.1464	20.6	20	0.607	1.61	0.414	0.995	0	0.947	1.02	1.00	0.999	10.0	16.1	-0.6
BR14-06-1			264	519	2.183	0.1652	12.3	15	0.821	0.503	0.591	0.999	0	0.922	0.980	1.00	1.00	40.0	20.1	0.9
Borabora sequer	nce C (i	16.50°S,	151.73°W)																	
BR18-01-1			271	389			8.3	15	1.07	0.867	0.611	0.998	0	1.03	0.944	1.00	1.00	20.0		
BR18-02-1			242	362	2.199	0.1827	9.1	15	1.01	0.870	0.628	0.998	0	1.01	1.01	1.00	1.00	20.0	17.4	6.6
BR18-04-2			214	325	I		9.9	15	0.942	0.804	0.572	1.00	0	0.966	1.11	1.00	1.00	20.0		
BR18-06-1	A	а	233	332	2.114	0.1764	10.7	15	1.02	0.843	0.593	0.999	0	0.992	1.03	1.00	1.00	20.0	16.9	0.3
BR18-07-1			250	358	2.076	0.1860	9.1	15	1.12	0.819	0.599	0.999	0	0.973	1.04	1.00	1.00	20.0	16.4	-0.1
BR18-08-1			304	407	2.217	0.1886	9.1	15	1.11	1.90	0.647	0.997	0	1.00	0.984	1.00	1.00	10.0	19.0	2.1
Tahaa sequence	A (16.6	58°S, 15,	$(.48^{\circ}W)$																	
TA03-02-1			301	359			11.5	20	0.330	0.291	0.046	0.966	15	0.941	1.04	0.908	0.999	10.0		
TA03-06-1			360	418			2.0	20	0.249	0.352	0.032	0.978	15	1.02	1.02	0.955	0.997	10.0		
TA02-08-1			79.5	424			7.4		No pr	imary comp	onent		25	0.833	0.954	0.705	0.998	40.0		
TA01-05-1			57.9	420			22.5		No pr	imary comp	onent		15	1.03	1.21	0.590	0.999	40.0		
TA01-07-1			47.4	433			20.0		No pr	imary comp	onent		25	0.868	1.29	0.439	0.998	40.0		
Tahaa sequence	B (16.6	58° S, 15.	1.45°W)																	
TA07-07-1			35.0	128			13.0	15	1.09	0.223	0.392	0.996	0	1.01	0.973	1.00	0.999	20.0	4.46	9.3
TA04-01-1			84.2	486			10.7	10	0.445	0.159	0.269	0.969	15	0.991	0.969	0.863	0.996	20.0		
TA04-08-1			61.5	324			18.0	20	0.337	0.657	0.543	0.972	0	1.03	0.975	1.00	0.997	10.0		
Tahaa sequence	C (16.t	56° S, 15.	1.44° W)	0													0000			
TA11-01-2			1500	288	1.846	0.3266	11.5	30	1.03	1.07	0.071	0.995	0	0.956	1.01	1.00	0.999	20.0		
TA11-02-2			940	191			17.4	20	0.848	3.47	0.132	0.979	0 0	0.983	1.02	1.00	0.996	10.0		
TA11-04-1 TA11-05-1	4		100	124	0/0		10./	07	0.842	4.23	0.110	0.989	<b>.</b> .	1.02	C/ 6.0	1.00	0000	10.0	2	-   -
1-C0-1141	n	ta	400	617	1.000	2/00.0	0.11	07	0.610	71.1	617.0	0.998	n d	106.0	10.901	1.961	9999	0.02	4.77	
TA11-06-2 TA11-07-1			204	191	186.2	/961.0	5.01 5.01	07	016.0	c1.1	0.244	200.0	0 0	1.07	0.986	1.00	0.000	20.0	23.0	-0.1
T410-07-1			4 F	107	C/0.1	7000.0	C.21	07	0.050	607.0	202.0	0.990		1.02	006.0	0.1.00	0000	10.0	6.07	-1.0
TA10-06-1 TA68-01-1	•		155 105	797	0	- 1150	0.27	30 35	0000	0.492	0.130	0.98/	01 0	1.021	166.0	0.05	0.999	40.0	2	-
TA08-01-1	A	to	1.6/	795	2.410	0.1222	10.01	07	0.8/1	1.48	1.14	199.0		1.02	0.000	1.00	1 00	0.02	0.67	2.10
TA 08 02 7			149	249 222	6/ C.7	0 1447	10.7	90	100.0	1.10	107.0	0.005		1.01	0200	1.00	1.00	0.02	0.22	0.6T
TA08-03-2 TA08-04-1			211	385			12.3	5 15	0.991	1.03	0.548	0.987		1.00	0.990	1.00	0.999	20.0	t.	<u>t</u>
TA08-05-1			301	354	2.346	0.1475	18.0	30	0.970	0.516	0.143	0.990	0	0.998	0.972	1.00	1.00	40.0		
TA08-05-2			260	386	2.346	0.1475	13.0	35	0.921	1.21	0.170	0.995	0	1.01	0.999	1.00	1.00	20.0	24.2	23.4
TA08-06-1			260	308	2.703	0.1379	14.5	25	0.849	0.949	0.189	0.995	0	0.985	1.03	1.00	1.00	20.0	19.0	28.8
TA08-07-2			289	321	2.428	0.1395	18.0	40	0.757	1.33	0.102	0.995	0	1.01	0.963	1.00	1.00	20.0		

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Table 2. (Cor.	tinued.																			
Sample ID	ΗT	LT	$NRM_0$	$ARM0_0$	$B_{ m rc}/B_{ m c}$	$M_{ m  IS}/M_{ m  s}$	LTD			First heating	50			S	econd heati	ng		$F_{\rm L}$	ц	ΔAIC
							(per cent)	$H_{\mathrm{L}}$	$Slope_A$	$Slope_N$	$f_{\rm N}$	$r_{\rm N}$	$H_{\mathrm{L}}$	$Slope_A$	$Slope_{T}$	$f_{\mathrm{T}}$	$r_{\mathrm{T}}$	$(\mu T)$	$(\mu T)$	
Tahaa sequence	e D (16.t	54°S, 15	1.44°W) 056	000			-	15	0.015	766.0	7120	0000	0	0000	0.015	001	1 00	0.01		
TA 10-05-1			92.0 85.1	308	1 503	03570	7.1	51 21	0.611	00270	0.710	0000	2 4	066.0	1.05	0.607	0.000	40.0	8 06	1 2
TA17-02-2w			28.0	264 264			5.7	20	0.290	0.387	0.647	0.989	0 0	1.04	0.953	1.00	0.996	10.0	2.9	<u>;</u>
TA17-04-1w			35.0	235	2.194	0.2801	5.7	30	0.233	0.650	0.532	0.995	0	1.10	0.972	1.00	0.998	10.0	6.50	-0.7
TA17-05-1	В		42.5	246	2.154	0.2615	5.7	15	0.407	0.485	0.633	0.995	20	0.985	0.982	0.932	0.997	10.0	4.85	9.3
TA17-06-1w			34.1	243			5.7	20	0.168	0.267	0.274	0.895	0	0.985	0.989	1.00	0.997	10.0		
TA17-07-1w			45.2	263			10.7	20	0.165	0.107	0.321	0.978	0	0.973	0.928	1.00	1.00	40.0		
TA16-03-2			105	378			9.1	20	0.707	0.271	0.113	0.973	0	1.00	0.980	1.00	0.997	10.0		
TA16-04-1			61.0	229	2.035	0.2468	10.7	20	0.683	0.339	0.173	0.995	0	1.00	1.00	1.00	0.999	10.0	3.39	-1.8
TA16-05-1	A	а	59.1	225	1.987	0.2539	13.8	15	0.717	0.333	0.216	0.996	0	0.999	1.02	1.00	0.998	10.0	3.33	-1.5
TA16-06-1			17.1	218	1.726	0.3126	9.9	20	0.983	0.275	0.802	0.995	0	1.02	1.02	1.00	0.999	10.0	2.75	-2.0
TA16-07-1			21.6	224	1.707	0.3147	10.7	20	0.962	0.260	0.603	0.995	0	1.02	1.01	1.00	0.999	10.0	2.60	-1.0
TA15-01-1		а	81.7	275	2.247	0.2045	7.4	10	0.866	0.768	0.934	0.995	5	0.983	0.998	0.980	1.00	10.0	7.68	18.5
TA15-02-2			87.3	278	2.193	0.2081	4.8	20	0.699	0.897	0.825	0.988	0	1.02	1.06	1.00	1.00	10.0		
TA15-02-3			91.0	276	2.193	0.2081	9.1	10	0.873	0.844	0.942	0.995	0	1.02	0.999	1.00	1.00	10.0	8.44	21.1
TA15-05-1			92.9	284	2.270	0.2043	7.4	20	0.778	0.445	0.634	0.984	0	1.03	1.01	1.00	1.00	20.0		
TA15-05-2			93.7	299	2.270	0.2043	6.5	5	0.996	0.714	0.988	0.995	0	1.01	1.05	1.00	0.999	10.0	7.14	26.5
TA15-06-1	A	а	74.3	315	2.464	0.1589	7.4	5	1.18	0.669	0.991	0.998	0	1.04	1.00	1.00	1.00	10.0	6.69	40.3
TA15-07-1			85.0	289	2.279	0.1925	4.8	5	1.07	0.686	0.995	0.995	0	0.984	1.03	1.00	1.00	10.0	6.86	23.1
Raiatea sequenc	3e A (16	.85°S, 1	51.37°W)																	
RT05-06-1			43.2	337	2.056	0.1975	10.7	20	0.536	0.260	0.621	0.995	0	1.01	0.969	1.00	0.999	20.0	5.20	14.4
RT10-01-2w			73.7	457	1.837	0.3167	9.1	15	0.312	0.384	0.479	0.995	0	0.990	1.01	1.00	0.999	10.0	3.84	23.1
RT10-01-3			24.9	409	1.837	0.3167	9.6	20	0.261	0.324	0.737	0.962	0	0.990	1.03	1.00	0.998	10.0		
RT10-02-1			32.7	409			14.5	20	0.261	0.332	0.488	0.964	0	1.01	1.05	1.00	0.999	10.0		
RT10-03-1	в		104	434	1.648	0.2840	9.1	25	0.225	0.577	0.330	0.995	0	0.996	0.953	1.00	0.997	10.0	5.77	-1.3
RT10-03-2	в		41.7	424	1.648	0.2840	9.1	15	0.327	0.308	0.661	0.995	0	0.993	1.02	1.00	0.997	10.0	3.08	18.4
Raiatea sequenc	3e B (16	.81°S, 1	51.39°W)																	
RT12-01-1m			147	398	2.349	0.2723	13.0	10	0.426	0.707	0.536	0.995	0	0.990	1.04	1.00	0.998	20.0	14.1	11.5
RT12-02-1m			130	331	1.899	0.2372	16.7	15	0.342	1.78	0.502	0.996	0	1.02	1.01	1.00	0.999	10.0	17.8	-2.0
RT12-03-2			113	455	2.234	0.2576	13.8	15	0.357	0.822	0.310	0.996	0	0.990	1.02	1.00	0.995	10.0	8.22	-1.5
RT12-04-1			92.8	460	2.000	0.2567	16.0	10	0.347	0.857	0.469	0.995	0	1.02	1.00	1.00	0.997	10.0	8.57	-1.9
RT12-04-2			92.2	417	2.000	0.2567	15.3	15	0.325	1.05	0.422	0.995	15	1.06	0.987	0.907	0.996	10.0	10.5	2.4
RT12-05-1	C	ပ	102	458	1.982	0.2405	13.8	10	0.446	0.913	0.523	0.997	10	1.00	0.998	0.927	0.998	10.0	9.13	15.3
RT12-06-2			110	436	1.903	0.2269	18.0	15	0.409	0.792	0.335	0.995	0	0.971	1.05	1.00	0.998	10.0	7.92	11.9
RT12-07-2			128	425	2.071	0.2405	17.4	30	0.473	0.768	0.217	0.997	10	0.982	1.05	0.930	0.999	10.0	7.68	4.5
Raiatea sequenc	2e C (16	6.85°S, 1	51.36°W)																	
RT18-02-2			137	364	1.500	0.3532	7.4	15	0.465	1.99	0.601	0.995	0	0.866	1.04	1.00	0.995	5.0	10.0	10.8
RT18-03-1			48.1	202	2.235	0.3721	5.7	20	0.681	0.331	0.506	0.990	0	0.835	0.912	1.00	0.999	20.0		
RT18-05-1	ц	e	74.6	215	1.760	0.3726	9.9	35	0.472	0.748	0.312	0.995	0	0.744	1.02	1.00	0.998	10.0	7.48	5.5
RT18-06-2			103	287	1.668	0.3494	14.5	10	0.442	0.924	0.764	0.996	25	0.940	1.01	0.788	0.999	10.0	9.24	16.1
RT18-07-1			79.1	253	1.942	0.3163	I	15	0.559	1.89	0.767	0.996	0	0.838	0.995	1.00	0.996	5.0	9.45	22.6
RT18-07-2m			218	462	1.942	0.3163	6.5	15	0.493	1.37	0.695	0.995	0	0.944	1.05	1.00	0.999	10.0	13.7	-2.0

Table 2. (Con	ntinued	(																		
Sample ID	HT	LT	$NRM_0$	$ARM0_0$	$B_{ m rc}/B_{ m c}$	$M_{ m rs}/M_{ m s}$	LTD		[	First heating	-			S	scond heati	gu		$F_{\rm L}$	н	AAIC
							(per cent)	$H^{\Gamma}$	$Slope_A$	Slope <sub>N</sub>	$f_{\rm N}$	$r_{\rm N}$	$H_{\mathrm{L}}$	$Slope_A$	$Slope_{T}$	$f_{\mathrm{T}}$	$r_{\mathrm{T}}$	$(\mu T)$	$(\mu T)$	
Huahine sequer.	ıce A (I	6.80°S,	151.01° W)				4	4	4							4	4	4		
HH01-02-2w			227	251	1.884	0.2350	9.9	40	0.692	4.47	0.320	0.992	0	1.01	1.04	1.00	1.00	10.0		
HH01-03-2			206	183	1 072	000	11.5	0 <del>1</del> 5	0.714	4.62	0.291	0.981	0 0	1.01	1.04	1.00	0.999	10.0		
HH01-04-2W HH01 06 1			607 202	157	C08.1	0.2310	10./	C 2 2 2	0.000	1.40	0.343	0.980	0 °C	1.02	1.04	0.602	0.000	0.05		
1-00-10111			107	017	1 007	1007.0	v.v v.o	000	C70.0	10.1 0C 1	107.0	166.0	C1 C	00.00	1.02	CU0.U	<i>466.</i> 0	20.0 20.0	107	0 00
			147	0/7	1.00/	1662.0	0.0	30	0.715	1.20	0.401	066.0		0000	1.02	1.00	0.000	0.00	1.00	0.02
HH04-05-1w			207	2.10 2.49	1.819	0.2989	3.8	cc 02	0./45	0.655	0.640	0.991		0.990 1.02	c0.1	1.00	1.00 1.00	40.0 40.0		
Huahine seauen	ce B (I	6.81°S.	151.00° W)	1				l					5							
HH11-01-2			222	520			9.1	15	0.800	0.592	0.209	0.995	0	0.828	0.737	1.00	0.998	30.0		
HH11-02-2			206	527	1.629	0.2391	11.5	15	0.394	0.751	0.216	0.995	20	0.814	1.02	0.703	0.995	20.0	15.0	19.5
HH11-03-2			192	486	1.608	0.2613	13.0	10	0.498	0.568	0.447	0.995	20	0.872	1.04	0.744	0.997	30.0	17.0	53.9
HH11-04-2	D	ပ	239	663	1.608	0.2506	6.5	15	0.496	0.668	0.263	0.995	25	0.893	1.02	0.694	0.997	20.0	13.4	18.6
HH11-04-2-2	D	c	297	717	1.608	0.2506	6.5	15	0.649	0.310	0.273	0.984	35	0.782	1.24	0.523	0.996	40.0		
HH11-05-2			228	633	1.574	0.2596	13.0	15	0.480	0.585	0.294	0.995	25	0.861	1.02	0.668	0.997	25.4	14.9	9.7
HH11-06-2			218	435		I	9.9	10	0.446	0.617	0.369	0.986	25	0.860	1.01	0.633	0.997	30.0		
HH11-07-1m	D		206	482	1.600	0.2368	9.9	10	1.17	0.710	0.426	0.995	0	0.909	0.955	1.00	0.998	40.0	28.4	21.0
HH11-07-2	D		221	599	1.600	0.2368	4.8	15	0.667	0.538	0.294	0.995	20	0.610	0.859	0.622	0.996	30.0		
HH10-01-1			114	361	1.785	0.2229	14.5	10	0.270	0.401	0.504	0.996	20	0.974	1.63	0.919	0.998	40.0		
HH09-01-2			363	454			5.7	10	1.12	0.976	0.892	0.998	0	1.08	1.06	1.00	1.00	20.0		
HH09-03-2			422	474	1.647	0.3349	2.9	10	1.12	0.961	0.903	0.998	0	1.05	1.05	1.00	1.00	20.0	19.2	8.7
HH09-04-1			367	393	1.735	0.3368	6.5	5	1.33	0.912	0.980	0.997	0	1.10	1.01	1.00	0.999	20.0	18.2	11.9
HH09-05-1			420	428	1.667	0.3413	3.8	0	1.31	0.367	1.00	0.998	0	1.09	1.10	1.00	1.00	50.0		
HH09-05-2			394	407	1.667	0.3413	2.0	5	1.33	0.853	0.976	0.998	0	1.08	1.02	1.00	1.00	20.0	17.1	0.0
HH09-06-1	A	а	391	411	1.714	0.3390	3.8	0	1.24	0.480	1.00	0.998	0	1.10	0.866	1.00	1.00	50.0		
HH09-06-2	Α	а	370	396	1.714	0.3390	1.0	0	1.42	0.853	1.00	0.998	0	1.08	1.05	1.00	1.00	20.0	17.1	3.1
HH09-06-2-1	A	а	378	400	1.714	0.3390	2.9	0	1.43	0.424	1.00	0.998	0	1.05	1.10	1.00	0.999	40.0		
HH09-07-2	A	а	366	417	1.706	0.3346	2.0	0	1.42	0.860	1.00	0.998	0	1.06	1.05	1.00	0.999	20.0	17.2	13.4
Huahine sequer	1) D-əəi	16.74°S,	$151.04^{\circ}W)$																	
HH16-01-2-2	В	а	304	275	1.603	0.2871	11.5	20	0.436	0.956	0.540	0.998	0	1.06	1.01	1.00	0.999	40.0	38.2	4.2
HH16-02-2			405	317	1.493	0.3320	5.7	20	0.634	1.20	0.550	0.999	0	0.991	1.05	1.00	1.00	30.0	36.0	10.4
HH16-03-1	A		402	311	1.692	0.2443	9.1	15	0.700	1.12	0.636	0.998	30	1.08	1.05	0.494	0.996	30.0	33.6	4.1
HH16-06-1		a	405	338	1.967	0.1992	9.1	10	0.917	0.988	0.824	0.998	30	1.08	1.04	0.446	0.998	30.0	29.6	7.2
HH16-07-2			381	317	1.921	0.2026	9.6	10	0.894	1.06	0.815	0.998	0	1.00	1.05	1.00	1.00	30.0	31.8	17.0
HH17-03-1			428	330	1.659	0.3589	7.4	15	0.602	1.03	0.652	0.999	30	0.993	1.71	0.996	0.639	40.0		
HH17-07-1			476	279	1.801	0.2355	10.7	15	0.845	0.973	0.623	0.997	0	1.02	1.08	1.00	1.00	40.0		
1-10-81HH			304	273	2.002	0.1789	13.8	15	0.802	0.785	0.313	0.999	0	0.949	1.16	1.00	0.999 0.1	40.0	.	;
1-10-07HH			460	2/4	168.1	0.2241	15.8	10	0.602	101	0.174	0.099	0 %	1.03	c0.1	1.00	1.00	40.0	58.1	14.9
	<		0.14	017	101		C.11	C 1 4	255.0	1.71	0.410	166.0	200	10.1	0.020	1.00	0.000	10.02		
ПП20-03-1 W	< <	, <del>G</del>	490 501	202 180	1.784	0.2466	12.0	01	600.0 2020	1.10	26C.U	0.000	o ç	1.05	00.0 20.1	0.1.00	0 000	40.0 25.4	101	12.7
HH20-03-2	V V	5 6	205	102	1 784	0.2466	0.01	20	0 306	1 36	0.304	0.980	45	1.67	0.638	0.230	0 003	40.0	1.2	
HH20-04-1	:	3	474	265			13.0	15	0.510	3.99	0.409	0.998	; o	1.01	1.08	1.00	666.0	10.0		
HH20-05-1w			463	262	1.823	0.2400	9.1	15	0.592	0.887	0.393	0.999	0	0.974	1.05	1.00	1.00	40.0	35.5	1.6
HH20-05-2			455	263	1.823	0.2400	12.3	15	0.555	1.02	0.420	0.999	0	0.987	1.09	1.00	1.00	40.0		
HH20-06-2			497	264	1.811	0.2177	12.3	15	0.497	3.98	0.394	0.997	20	1.05	1.04	0.756	0.997	10.0	39.8	-1.2
HH20-07-2			497	270			9.6	10	0.638	1.90	0.541	1.00	0	1.01	1.09	1.00	1.00	20.0		
HH19-03-1			399	307	1.882	0.2228	10.7	15	0.812	0.946	0.540	0.998	35	0.997	1.52	0.223	0.997	40.0	[	
HH19-06-1			428	284	1.913	0.2078	10.7	15	0.867	0.951	0.578	0.997	20	0.974	1.20	0.580	0.999	40.0		
HH21-01-1			358	437	1.746	0.3369	12.3	35	0.805	0.518	0.220	0.996	5	0.953	1.15	0.962	0.999	40.0		

Geomagnetic field intensity during the last 5 Myr 89

	00 200 128 62	00 20.0 13.8 6.3 00 40.0 14.1 12.9	00         20.0         13.8         6.3           00         40.0         14.1         12.9           09         20.0         15.8         5.0	00         20.0         13.8         6.3           00         40.0         14.1         12.9           09         20.0         15.8         5.0           09         40.0         15.8         5.0	00         20.0         13.8         6.3           00         40.0         14.1         12.9           99         20.0         15.8         5.0           99         40.0         15.8         -1.8           99         20.0         15.8         -1.6           99         20.0         15.5         -1.5	00         20.0         13.8         6.3           00         40.0         14.1         12.9           099         20.0         15.8         5.0           099         40.0         15.8         -1.8           099         20.0         15.8         -1.6           099         20.0         15.5         -1.5           099         10.0         7.55         20.4	00         20.0         13.8         6.3           00         40.0         14.1         12.9           099         20.0         15.8         5.0           099         40.0         15.8         -1.8           099         20.0         15.8         -1.8           099         20.0         15.5         -1.5           099         10.0         7.55         20.4           00         10.0         -         -	00         20.0         13.8         6.3           00         40.0         14.1         12.9           099         20.0         15.8         5.0           099         40.0         15.8         -1.8           099         20.0         15.8         -1.8           099         20.0         15.5         -1.5           099         10.0         7.55         20.4           00         10.0         -         -           099         10.0         -         -	00         20.0         13.8         6.3           00         40.0         14.1         12.9           099         20.0         15.8         5.0           099         40.0         15.8         -1.8           099         20.0         15.8         -1.15           099         20.0         15.5         -1.5           099         10.0         7.55         20.4           00         10.0         7.55         20.4           099         10.0         11.4         11.4	00         20.0         13.8         6.3           00         40.0         14.1         12.9           099         20.0         15.8         5.0           099         20.0         15.8         5.0           099         20.0         15.8         5.0           099         20.0         15.8         -1.8           099         10.0         7.55         -1.5           099         10.0         7.55         20.4           099         10.0         -1.6         -0.0           099         10.0         -1.6         -0.0           000         10.0         -1.4         11.4           000         10.0         -1         -0           000         10.0         -1         -0	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
	1 00 1	1.00 1.00 1.00 1.00	1.00 1.00 1.00 1.00 0.963 0.99	1.00         1.00           1.00         1.00           0.963         0.99           1.00         0.99	1.00         1.00           1.00         1.00           1.00         1.00           0.963         0.99           1.00         0.99           1.00         0.99	1.00         1.00           1.00         1.00           0.963         0.99           1.00         0.99           1.00         0.99           1.00         0.99           1.00         0.99           1.00         0.99	1.00         1.00           1.00         1.00           0.963         0.99           1.00         0.99           1.00         0.99           1.00         0.99           1.00         0.99           1.00         0.99           1.00         0.99           1.00         1.00           1.00         1.00	1.00         1.00           1.00         1.00           1.00         1.00           0.963         0.99           1.00         0.99           1.00         0.99           1.00         0.99           1.00         0.99           1.00         0.99           1.00         1.00           1.00         1.00           1.00         1.00           1.00         1.00	1.00         1.00           1.00         1.00           1.00         1.00           0.963         0.996           0.100         0.99           1.000         0.99           1.000         0.99           1.000         0.99           1.000         0.99           1.000         0.99           1.000         0.99           1.000         1.00           1.000         1.00           1.000         0.99	1.00         1.00           1.00         1.00           1.00         1.00           0.963         0.996           0.100         0.99           1.000         0.99           1.000         0.99           1.000         0.99           1.000         0.99           1.000         1.00           1.000         1.00           1.000         1.00           1.000         1.00           1.001         0.01	1.00         1.00           1.00         1.00           1.00         1.00           0.963         0.963           0.963         0.99           1.00         0.99           1.00         0.99           1.00         0.99           1.00         0.99           1.00         0.99           1.00         0.99           1.00         0.99           1.00         0.99           1.00         1.00           1.00         0.99           1.00         0.99           1.00         0.99           1.00         0.99	1.00         1.00           1.00         1.00           1.00         1.00           0.963         0.963           0.963         0.99           1.00         0.99           1.00         0.99           1.00         0.99           1.00         0.99           1.00         1.00           1.00         1.00           1.00         1.00           1.00         1.00           1.00         1.00           1.00         0.99           1.00         1.00           1.00         1.00           1.00         1.00	1.00         1.00           1.00         1.00           0.963         0.99           0.963         0.99           1.00         0.99           1.00         0.99           1.00         0.99           1.00         0.99           1.00         0.99           1.00         0.99           1.00         0.99           1.00         0.99           1.00         0.99           1.00         0.99           1.00         0.99           1.00         0.99           1.00         0.99           1.00         0.99           1.00         0.99           1.00         0.99           1.00         0.99           1.00         0.99	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
		0.997 1.05	0.997 1.05 1.05	0.997 1.05 1.05 1.01	0.997 1.05 1.05 1.01 1.01	0.997 1.05 1.05 1.01 1.01 1.01	0.997 1.05 1.05 1.01 1.01 1.04 1.04	0.997 1.05 1.05 1.01 1.01 1.01 1.04 1.03 0.951	0.997 1.05 1.05 1.01 1.01 1.01 1.04 1.03 0.951 0.955	0.997 1.05 1.05 1.01 1.01 1.01 1.04 1.03 0.951 0.951 0.953	0.997 1.05 1.05 1.01 1.01 1.04 1.04 1.03 0.951 0.957 0.870	0.997 1.05 1.05 1.01 1.01 1.04 1.04 1.03 0.951 0.957 0.987 0.800 1.02	0.997 1.05 1.05 1.01 1.01 1.04 1.03 0.955 0.995 0.995 0.987 0.987 0.989	0.997 1.05 1.05 1.01 1.01 1.04 1.03 0.995 0.995 0.987 0.987 0.987 0.989 1.02	0.997 1.05 1.05 1.01 1.01 1.04 1.03 0.995 0.995 0.995 0.987 0.987 0.987 0.987 1.02 1.02	0.997 1.05 1.05 1.01 1.01 1.04 1.03 0.955 0.955 0.957 0.987 0.987 0.987 0.987 0.987 0.987 1.02 1.02	0.997 1.05 1.05 1.01 1.01 1.01 1.04 1.03 0.955 0.957 0.957 0.987 0.987 0.989 1.02 1.02 1.02 1.02 1.02 1.02 0.989 0.989 0.989 0.989 0.999 0.999	0.997 1.05 1.05 1.01 1.01 1.01 1.04 1.03 0.955 0.955 0.995 0.987 0.987 0.987 0.989 1.02 1.02 1.02 1.02 1.02 0.989 0.989 0.999 0.995 0.999 0.995 0.995 0.999 0.995 0.995 0.987 0.987 0.987 0.987 0.987 0.987 0.989 0.989 0.985 0.989 0.989 0.989 0.989 0.985 0.989 0.989 0.985 0.989 0.989 0.985 0.989 0.989 0.985 0.989 0.989 0.999 0.999 0.995 0.995 0.999 0.995 0.995 0.995 0.999 0.995 0.99	0.997 1.05 1.05 1.01 1.01 1.01 1.01 1.03 0.955 0.955 0.957 0.995 0.987 0.989 1.02 1.02 1.02 1.02 0.989 0.989 0.985 0.989 1.02 1.02 1.02 0.989 1.02 1.05 1.05 0.985	0.997 1.05 1.05 1.01 1.01 1.01 1.04 1.03 0.955 0.955 0.955 0.955 0.959 0.989 1.02 1.02 1.02 1.02 1.02 1.02 1.02 1.02	0.997 1.05 1.01 1.01 1.01 1.04 1.03 0.995 0.987 0.989 0.989 0.989 0.985 1.01 1.01 1.01 1.01 1.01 1.01	$\begin{array}{c} 0.997\\ 1.05\\ 1.01\\ 1.01\\ 1.01\\ 1.03\\ 1.03\\ 0.995\\ 0.987\\ 0.987\\ 0.987\\ 0.987\\ 0.999\\ 0.989\\ 1.02\\ 1.0$	$\begin{array}{c} 0.997\\ 1.05\\ 1.05\\ 1.01\\ 1.01\\ 1.01\\ 1.03\\ 1.03\\ 0.995\\ 0.995\\ 0.995\\ 0.995\\ 0.987\\ 0.999\\ 0.989\\ 1.02\\ 1.02\\ 1.02\\ 1.02\\ 1.02\\ 1.02\\ 1.02\\ 1.02\\ 1.02\\ 0.985\\ 0.988\\ 0.981\\ 0.098\\ 0.981\\ 0.98$	$\begin{array}{c} 0.997\\ 1.05\\ 1.05\\ 1.01\\ 1.01\\ 1.01\\ 1.03\\ 1.03\\ 0.995\\ 0.995\\ 0.987\\ 0.995\\ 0.989\\ 0.999\\ 0.999\\ 0.999\\ 0.999\\ 0.981\\ 1.01\\ 1.02\\ 1.02\\ 1.02\\ 1.02\\ 0.999\\ 0.993\\ $	0.997 1.05 1.01 1.01 1.01 1.01 1.04 1.02 0.995 0.987 0.995 0.989 1.02 1.02 1.02 1.02 1.02 1.02 1.02 1.02 1.02 1.02 1.02 1.02 1.02 1.02 0.989 0.999 0.999 0.993 0.991 0.931 0.931 0.932 0.993 0.994 0.99	0.997 1.05 1.01 1.01 1.01 1.01 1.03 0.951 0.957 0.995 0.987 0.987 0.989 1.02 1.02 1.02 1.02 1.02 1.02 1.02 1.02 1.02 1.02 1.02 1.02 0.999 0.999 0.999 0.999 0.999 1.02 1.03 1.02	0.997 1.05 1.01 1.01 1.01 1.04 1.04 1.03 0.951 0.955 0.955 0.957 0.987 0.987 0.989 0.999 0.999 0.999 0.999 0.999 0.993 0.993 0.941 1.00 0.941 0.942	0.997 1.05 1.01 1.01 1.01 1.02 0.951 0.955 0.955 0.956 0.987 0.987 0.987 0.989 0.989 0.989 0.999 0.999 0.985 0.985 0.999 0.981 0.981 0.981 0.930 0.942 0.930 0.942 0.930	0.997 1.05 1.01 1.01 1.01 1.01 1.03 0.995 0.995 0.987 0.987 0.987 0.987 0.987 0.987 0.987 0.987 0.980 0.981 0.993 0.942 0.942 0.930	0.997 1.05 1.01 1.01 1.01 1.01 1.03 0.995 0.995 0.987 0.987 0.987 0.987 0.989 0.999 0.999 0.999 0.993 0.993 0.993 0.993 0.993 0.981 0.930 0.931 0.932 0.934 0.934 0.934 0.934 0.934 0.934 0.934 0.934 0.934 0.954	0.997 1.05 1.01 1.01 1.01 1.01 1.03 0.995 0.995 0.987 0.987 0.987 0.989 0.999 0.999 0.999 0.981 0.942 0.941 1.02 0.993 0.993 0.942 0.931 0.931 0.931 0.932 0.931 0.932 0.931 0.932 0.931 0.932 0.931 0.932 0.931 0.932 0.931 0.932 0.931 0.932	0.997 1.05 1.01 1.01 1.01 1.01 1.03 0.995 0.995 0.987 0.987 0.987 0.999 0.999 0.999 0.999 0.993 0.981 1.02 1.02 1.02 0.993 0.993 0.993 0.993 0.981 0.931 0.932 0.933 0.931 0.932 0.933 0.931 0.932 0.931 0.932 0.933 0.933 0.932 0.933 0.934 0	0.997 1.05 1.01 1.01 1.01 1.01 1.02 0.995 0.987 0.987 0.995 0.989 0.999 0.999 0.981 1.02 1.02 1.02 1.02 1.02 1.02 0.999 0.999 0.981 0.930 0.930 0.931 0.932 0.934 0.932 0.934 0.93	0.997 1.05 1.01 1.01 1.01 1.01 1.04 1.03 0.995 0.987 0.987 0.987 0.987 0.989 0.989 0.999 0.989 0.999 0.981 1.02 1.02 1.02 1.02 1.02 0.999 0.993 0.981 0.930 0.930 0.930 0.931 0.931 0.932 0.931 0.932 0.93
1	101	0 1.01 0 0.939	0 1.01 0 0.939 5 0.931	0 1.01 0 0.939 5 0.931 0 0.956	0 1.01 0 0.939 5 0.931 0 0.956 0 0.978	0 1.01 0 0.939 5 0.931 0 0.956 0 0.978 0 1.02	0 1.01 0 0.939 5 0.931 0 0.956 0 0.978 0 1.02 0 1.01	0 1.01 0 0.939 5 0.931 0 0.956 0 0.978 0 1.02 0 1.01 0 1.02	0 1.01 0 0.939 5 0.931 0 0.956 0 0.978 0 1.02 0 1.02 0 1.02 0 0.992	0 1.01 0 0.939 5 0.931 0 0.956 0 0.978 0 1.02 0 1.02 0 1.02 0 0.992 0 0.978	0 11.01 5 0.939 5 0.931 0 0.978 0 0.978 0 1.02 0 1.02 0 0.978 0 0.978 0 0.978	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	0 1.01 5 0.933 6 0.936 0 0.978 0 0.978 0 1.01 0 1.02 0 1.02 0 0.992 0 0.992 0 0.992 0 0.992 0 0.985 0 0.985 0 0.985 0 0.985 0 0.985 0 0.985 0 0.985 0 0.985 0 0.985 0 0.091 0 0.095 0 0.005 0 0.005 0 0.095 0 0.005 0 0.005	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
	0,000	0.996	866.0 9996 0.998	0.998 0.998 0.999	8900 8000 8000 8000 8000 8000 8000 8000	0.998 0.998 0.999 0.995 0.995	0.998 0.998 0.999 0.999 0.995 0.995	0.998 0.998 0.997 0.995 0.995 0.988 0.971	0.998 0.998 0.997 0.995 0.995 0.971 0.971 0.958	0.998 0.995 0.997 0.995 0.995 0.971 0.995 0.995	0.998 0.995 0.995 0.995 0.995 0.995 0.993 0.993	0.998 0.999 0.995 0.995 0.995 0.995 0.995 0.995 0.995	0.998 0.999 0.995 0.995 0.995 0.995 0.995 0.993 0.993 0.993	0.998 0.995 0.995 0.995 0.995 0.995 0.993 0.993 0.993 0.983	0.998 0.995 0.995 0.995 0.995 0.995 0.995 0.995 0.995 0.995 0.995 0.995	0.998 0.995 0.995 0.995 0.995 0.995 0.995 0.995 0.995 0.995 0.995	0.998 0.999 0.995 0.995 0.995 0.995 0.995 0.995 0.995 0.995 0.995 0.995 0.995	0.998 0.999 0.995 0.995 0.993 0.993 0.993 0.993 0.995 0.995 0.995 0.995 0.995	0.998 0.995 0.995 0.995 0.995 0.995 0.995 0.995 0.995 0.995 0.995 0.995	0.998 0.999 0.995 0.995 0.995 0.995 0.995 0.995 0.995 0.995 0.995 0.995 0.995 0.995 0.995	0.998 0.999 0.995 0.995 0.995 0.995 0.995 0.995 0.995 0.995 0.995 0.995 0.995 0.995 0.995	0.998 0.999 0.995 0.995 0.995 0.995 0.995 0.995 0.995 0.995 0.995 0.995 0.995 0.995 0.995 0.995 0.995	0.998 0.999 0.995 0.995 0.995 0.995 0.995 0.995 0.995 0.995 0.995 0.995 0.995 0.995	0.998 0.999 0.995 0.995 0.995 0.995 0.995 0.995 0.995 0.995 0.995 0.995 0.995 0.995 0.995 0.995 0.995 0.995 0.995	0.998 0.999 0.995 0.995 0.995 0.995 0.995 0.995 0.995 0.995 0.995 0.995 0.995 0.995 0.995 0.995 0.995	0.998 0.999 0.995 0.995 0.995 0.995 0.995 0.995 0.995 0.995 0.995 0.995 0.995 0.995 0.995 0.995 0.995 0.995 0.995	0.998 0.999 0.995	0.998 0.999 0.995 0.999 0.995 0.995 0.995 0.995 0.995 0.995 0.995 0.995 0.995 0.995 0.995 0.995 0.995 0.995 0.995 0.995 0.995 0.995	0.998 0.999 0.995 0.995 0.995 0.995 0.995 0.995 0.995 0.995 0.995 0.995 0.995 0.995 0.995 0.995 0.995 0.995 0.995 0.995	0.998 0.999 0.999 0.995 0.995 0.995 0.995 0.995 0.995 0.995 0.995 0.995 0.995 0.995 0.995 0.995 0.995 0.995 0.995	0.998 0.999 0.995 0.995 0.995 0.995 0.995 0.995 0.995 0.995 0.995 0.995 0.995 0.995 0.995 0.995 0.995 0.995 0.995	0.998 0.999 0.999 0.995	0.998 0.999 0.999 0.995	0.998 0.999 0.995
	0102 0 201	592 0.791 352 0.829	<ul><li>592 0.791</li><li>352 0.829</li><li>790 0.592</li></ul>	<ul> <li>592 0.791</li> <li>352 0.829</li> <li>790 0.592</li> <li>396 0.634</li> </ul>	<ul> <li>592 0.791</li> <li>352 0.829</li> <li>790 0.592</li> <li>396 0.634</li> <li>777 0.676</li> </ul>	592         0.791           352         0.829           790         0.592           336         0.634           777         0.676           755         1.00	592         0.791           352         0.829           790         0.592           396         0.634           777         0.676           755         1.00           .90         1.00	592         0.791           352         0.829           790         0.592           396         0.634           777         0.676           755         1.00           90         1.00           97         0.992	592         0.791           352         0.829           790         0.592           396         0.634           777         0.676           755         1.00           90         1.00           .97         0.992           .97         0.992           .97         0.992           .100         1.00	592         0.791           352         0.829           790         0.592           396         0.654           777         0.676           777         0.676           790         1.00           90         1.00           97         1.00           97         1.00           97         1.00           97         1.00           97         1.00	592         0.791           352         0.829           790         0.592           777         0.676           777         0.676           755         1.00           777         0.676           90         1.00           97         0.992           1.44         1.00           0.66         1.00           0.67         1.00           0.77         0.614           0.77         0.614           1.00         1.00	592         0.791           352         0.829           790         0.592           777         0.676           777         0.676           777         0.676           755         1.00           777         0.676           777         0.676           777         0.676           1.00         1.00           47         1.00           66         1.00           67         1.00           859         1.00	592         0.791           352         0.829           790         0.592           777         0.656           777         0.676           777         0.676           777         0.676           90         1.00           1.14         1.00           4.7         1.00           66         1.00           747         1.00           747         1.00           747         1.00           747         1.00           747         1.00           75         1.00	592         0.791           352         0.829           790         0.592           396         0.534           777         0.676           777         0.676           777         0.676           90         1.00           97         0.902           114         1.00           124         1.00           131         1.00           147         1.00           181         1.00	592         0.791           352         0.829           790         0.592           396         0.534           777         0.676           777         0.676           777         0.676           790         1.00           97         1.00           97         1.00           97         1.00           114         1.00           124         1.00           131         1.00           859         1.00           889         0.983	592     0.791       352     0.829       770     0.654       777     0.676       777     0.676       775     1.00       775     1.00       97     0.992       114     1.00       876     1.00       777     0.676       777     0.676       777     0.676       777     1.00       114     1.00       120     1.00       131     1.00       181     1.00       386     0.983	592         0.791           352         0.829           770         0.654           777         0.676           775         1.00           775         1.00           997         0.676           907         0.692           907         0.692           907         1.00           97         0.992           114         1.00           124         1.00           138         1.00           181         1.00           181         0.993           386         0.833	592         0.791           582         0.829           770         0.654           777         0.676           777         0.676           790         0.592           777         0.676           797         0.902           99         1.00           97         1.00           747         0.676           747         1.00           747         1.00           747         1.00           885         1.00           181         1.00           181         0.933           338         0.9303           333         0.436	592         0.791           552         0.829           770         0.676           777         0.676           777         0.676           777         0.676           777         0.676           777         0.676           777         0.676           747         0.676           700         1.00           97         1.00           97         1.00           859         1.00           181         1.00           338         0.833           338         0.833           333         0.436           832         1.00	592         0.791           582         0.829           790         0.592           790         0.544           777         0.676           777         0.676           777         0.676           777         0.676           99         1.00           97         1.00           97         1.00           97         1.00           97         1.00           97         1.00           97         1.00           97         1.00           9859         1.00           181         1.00           181         1.00           338         0.8339           338         0.9933           333         0.4366           333         0.4366           333         0.4366	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	592         0.791           552         0.829           770         0.676           777         0.676           777         0.676           777         0.676           777         0.676           777         0.676           777         0.676           755         1.00           97         0.992           114         1.00           47         1.00           859         1.00           859         1.00           8859         1.00           8832         1.00           8832         1.00           181         1.00           8832         0.933           0.436         0.697           0.66         0.619	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
	2 0 202 0	0.696 0.6 0.772 0.3	0.696 0.6 0.772 0.3 0.465 0.7	0.696         0.6           0.772         0.3           0.465         0.7           0.482         0.3	0.696         0.6           0.772         0.3           0.465         0.7           0.482         0.3           0.482         0.3           0.444         0.7	0.696 0.6 0.772 0.3 0.465 0.7 0.482 0.7 0.482 0.3 0.444 0.7 1.08 0.7	0.696 0.6 0.772 0.3 0.465 0.7 0.482 0.3 0.444 0.7 1.08 0.7 1.01 1.5	0.696 0.696 0.6 0.772 0.3 0.465 0.7 0.482 0.3 0.482 0.3 0.444 0.7 1.08 0.7 1.08 0.7 1.01 1.5 0.882 1.5	0.696 0.696 0.6 0.772 0.3 0.465 0.7 0.482 0.3 0.444 0.7 1.08 0.7 1.08 0.7 1.01 1.5 0.882 1.5 0.968 1.5	$\begin{array}{c} 0.696 & 0.696 \\ 0.772 & 0.372 \\ 0.465 & 0.7 \\ 0.482 & 0.3 \\ 0.444 & 0.7 \\ 1.08 & 0.7 \\ 1.01 & 1.2 \\ 1.01 & 1.2 \\ 0.882 & 1.3 \\ 0.968 & 1.3 \\ 1.09 & 1.4 \end{array}$	$\begin{array}{c} 0.696 & 0.696 \\ 0.772 & 0.372 \\ 0.465 & 0.7 \\ 0.482 & 0.3 \\ 0.444 & 0.7 \\ 0.444 & 0.7 \\ 1.08 & 0.7 \\ 1.01 & 1.6 \\ 0.368 & 1.1 \\ 0.968 & 1.1 \\ 0.943 & 1.1 \\ 0.943 & 1.1 \end{array}$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
	10	10	10 10	10 10 10 10	01 01 01 01 01	0 0 0 0 0 0 0	0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0000000000	000000000000	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	999990000000	9999900000000000	0 0 0 0 0 0 0 v 0 0 0 0 v	0 0 0 0 0 0 0 v 0 0 0 0 0 v <u>v</u>	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	20 v 12 v 0 0 0 0 v 0 0 0 v 12 v 25	20 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	1, 2, 2, 2, 2, 2, 0, 0, 0, 0, 0, 0, 0, 0, 0, 0, 0, 0, 0,	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0	10 10 10 10 10 10 10 10 10 10	0 0 0 0 0 0 0 0 0 0 0 0 0 0	10 10 10 10 10 10 10 10 10 10	0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	10 10 10 10 10 10 10 10 10 10
	115	14.5 16.0	14.5 16.0 15.3	14.5 16.0 15.3 16.7	14.5 16.0 15.3 16.7 14.5	14.5 16.0 15.3 16.7 14.5 5.7	14.5 16.0 15.3 16.7 14.5 5.7 6.7	14.5 16.0 15.3 16.7 5.7 5.7 3.8	14.5 16.0 15.3 16.7 5.7 6.7 3.8 9.9	14.5 16.0 16.7 16.7 5.7 6.7 8.8 8.3	14.5 16.0 115.3 16.7 5.7 5.7 6.7 8.3 8.3 8.3	14.5 16.0 16.7 16.7 5.7 6.7 8.3 8.3 8.3 9.9	14.5 16.0 15.3 16.7 5.7 5.7 6.7 8.3 8.3 8.3 9.9 9.9	14.5 16.0 15.3 16.7 5.7 7.7 5.7 7.8 8.3 8.3 8.3 9.9 9.9	14.5 16.0 15.3 16.7 5.7 5.7 5.7 8.3 8.3 9.9 9.9 13.8 13.8	14.5 16.0 16.7 16.7 5.7 5.7 6.7 8.3 8.3 9.9 9.9 9.9 12.3	14.5 16.0 16.7 14.5 14.7 14.5 14.5 14.5 14.5 14.5 14.5 14.5 11.5 11	14.5 16.0 16.7 14.5 14.5 14.5 14.5 14.5 14.5 14.5 14.5	14.5 16.0 16.7 16.7 16.7 16.7 16.7 16.7 16.7 16.7	14.5 16.0 16.7 16.7 16.7 16.7 16.7 16.7 16.7 16.7	14.5 16.0 16.7 16.7 16.7 16.7 16.7 16.7 16.7 16.7	14.5 16.0 16.7 16.7 16.7 16.7 16.7 16.7 16.7 16.7	14.5 16.0 16.7 16.7 16.7 16.7 16.7 16.7 16.7 16.7	14.5 16.0 16.7 16.7 16.7 16.7 16.7 16.7 16.7 16.7	14.5 16.0 16.1 16.7 14.5 14.5 14.5 14.5 14.5 11.5 11.5 11.5	14.5 16.0 16.0 14.5 14.5 14.5 14.5 14.5 14.5 14.5 11.5 11	14.5 16.0 16.1 16.7 14.5 14.5 14.5 14.5 14.5 14.5 14.5 11.5 11	14.5 16.0 16.0 16.7 16.7 16.0 16.0 16.0 16.0 16.0 16.0 16.0 11.5 11.5 11.5 11.5 11.5 11.5 20.0 20.0	14.5 16.0 16.7 16.7 16.7 16.7 16.7 16.7 16.7 16.7	14.5 16.0 16.7 16.7 16.7 16.7 16.7 16.7 16.7 16.7	14.5 16.0 16.7 16.7 16.7 16.7 16.7 16.7 16.7 16.7	14.5 16.0 16.7 16.7 16.7 16.7 16.7 16.7 16.7 16.7	14.5 16.0 16.0 16.1 16.1 14.5 14.5 14.5 14.5 14.5 11.5 11.5 11	14.5 16.0 16.0 16.1 16.1 16.0 11.5 16.0 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11
0 1751	10/1.0	0.1791	0.1791 0.2359	0.1791 0.2359 0.2418	0.1791 0.2359 0.2418 0.2226	0.1791 0.2359 0.2418 0.2226	0.1791 0.2359 0.2418 0.2226 	0.1791 0.2359 0.2418 0.2226 	0.1791 0.2359 0.2418 0.2226 	0.1791 0.2359 0.2418 0.2226 	0.1791 0.2359 0.2418 0.2226 	0.1791 0.2359 0.2418 0.2226   0.3310	0.1791 0.2359 0.2359 0.2226   0.3310 0.2429	0.1791 0.2359 0.2418 0.2226   0.3310 0.2429	0.1791 0.2359 0.2418 0.2226   0.2320 0.2429 0.2429 0.2184	0.1791 0.2359 0.2418 0.2226   0.2310 0.2429 0.2184 0.2184	0.1791 0.2359 0.2418 0.2226   0.2310 0.2429 0.2429 0.2699	0.1791 0.2359 0.2359 0.2226 0.2226 0.2226 0.2310 0.2429 0.2429 0.2429	0.1791 0.2359 0.2359 0.2418 0.2226 0.2310 0.2429 0.2429 0.2184 0.2659	0.1791 0.2359 0.2359 0.2226 0.2226 0.23310 0.2184 0.2184 0.2184 0.2552 0.2699	0.1791 0.2359 0.2418 0.2226  0.2226 0.22429 0.2429 0.2184 0.2552 0.2699	0.1791 0.2359 0.2418 0.2226   0.2184 0.2184 0.2552 0.2699 	0.1791 0.2359 0.2359 0.2226 0.2226 0.2184 0.2184 0.2184 0.2699 0.2699	0.1791 0.2359 0.2359 0.2226 0.2226 0.2310 0.2429 0.2184 0.2184 0.2552 0.2699	0.1791 0.2359 0.2418 0.2226  0.2226 0.2184 0.2184 0.2699 	0.1791 0.2359 0.2359 0.2226 0.2226 0.2310 0.2429 0.2429 0.2429 0.2699 0.2699 0.2552 0.2699 0.2699 0.2552 0.2552 0.2552	0.1791 0.2359 0.2359 0.2218 0.2226 0.23310 0.23310 0.2429 0.2429 0.2429 0.2429 0.26599 0.26599 0.26599 0.26599 0.26599 0.26516 0.26516 0.26516 0.26516 0.26516 0.26516 0.26516 0.26516 0.26516 0.26516 0.27516 0.26516 0.27516	0.1791 0.2359 0.2359 0.2358 0.2226 0.23310 0.22429 0.2184 0.2552 0.26599 0.26599 0.26599 0.26599 0.26599 0.26590 0.26590 0.26590 0.26590 0.26590 0.26590 0.26590 0.26590 0.26590 0.26590 0.26590 0.26500 0.26500 0.26500 0.26500 0.26500 0.26500 0.275000 0.27500 0.27500 0.27500 0.27500 0.27500 0.27500 0.27500 0.27500 0.27500 0.27500 0.27500 0.27500 0.27500000000000000000000000000000000000	0.1791 0.2359 0.2359 0.2226 0.2226 0.23310 0.22429 0.2184 0.2184 0.2552 0.2699 0.2569 0.2552 0.2699 0.2568 0.2552 0.2569 0.2568 0.2669 0.2669 0.2669 0.2669 0.2669 0.2669 0.2669 0.2669 0.2669 0.2668 0.2668 0.2669 0.26688 0.266888 0.266888 0.266888 0.266888 0.266888 0.266888 0.2668888 0.26688888 0.2668888888888 0.26688888888888888888888888888888888888	0.1791 0.2359 0.2359 0.2226 0.2226 0.23310 0.22429 0.2184 0.2552 0.2699 0.2569 0.2569 0.2552 0.2699 0.1516 0.1516 0.1548 0.1548	0.1791 0.2359 0.2359 0.2226 0.23310 0.2226 0.22429 0.2429 0.2552 0.2699 0.2552 0.2699 0.2552 0.2699 0.1516 0.1516 0.1548 0.1548 0.1556	0.1791 0.2359 0.2418 0.2256 0.2226 0.2359 0.2429 0.2552 0.2699 0.2552 0.2699 0.1516 0.1516 0.1548 0.1556 0.1556 0.1556	0.1791 0.2359 0.2418 0.2226 0.2226 0.22429 0.2552 0.2552 0.2552 0.2552 0.2552 0.2552 0.2552 0.2552 0.2552 0.2552 0.2552 0.25550 0.25550 0.25550 0.25550000000000	0.1791 0.2359 0.2359 0.2226 0.2310 0.2310 0.23310 0.23310 0.2352 0.2429 0.2429 0.2552 0.2429 0.2552 0.2699 0.1516 0.1516 0.1548 0.1556 0.1548 0.1556
2266 26	20 2.174 07 2.174		01 2.094	01 2.094 85 2.128	01 2.094 85 2.128 80 1.981	01 2.094 85 2.128 80 1.981 59 —	01 2.094 85 2.128 80 1.981 07 —	01 2.094 85 2.128 80 1.981 59 51 51	01 2.094 85 2.128 80 1.981 59 – – 07 – – 31 – –	00 2.004 85 2.128 86 1.981 59 1.981 71 1.981 731 1.981 51 1.981 51 2.004 51 2.004 52 2.128 53 2.128 54 2.004 55 2.128 56 2.128 57 2.128 58 2.128 58 2.128 58 2.128 58 2.128 58 2.128 58 2.128 58 2.128 58 2.128 59 2.128 59 2.128 50 2.128 51 2.128 51 2.128 52 2.128 52 2.128 52 2.128 53 2.128 53 2.128 54 2.128 55 2.128 56 2.128 57	01 2.094 85 2.128 86 1.981 75 1.991 75	01 2.094 85 2.128 86 1.981 71 1.545 71 1.545	00 2.004 85 2.128 80 1.981 59 1.981 51 1.581 51 1.545 97 1.764	01     2.004       85     2.128       80     1.981       59     1.981       331     1.981       551     1       553     1.545       71     1.545       97     1.764	01     2.004       85     2.128       80     1.981       59     -       07     -       51     -       55     -       51     -       53     -       54     -       53     -       54     -       53     -       54     -       71     1.545       97     1.764       83     1.870	01     2.094       85     2.128       80     1.981       59     1.981       51     1       53     1       54     1.545       97     1.545       83     1.545       71     1.545       83     1.643       73     1.689       73     1.689	01       2.094         85       2.128         80       1.981         59       1.981         67       1.981         73       1.545         71       1.545         97       1.545         83       1.870         18       1.689         13       1.689         168       1.687	01       2.094         88       2.128         89       1.981         59       1.981         67       1.981         51       1.         53       1.545         97       1.545         83       1.545         71       1.545         83       1.687         18       1.687         13       1.687	01       2.004         88       2.128         89       1.981         59       1.981         61       331         62       1.981         63       1.1545         71       1.545         73       1.545         73       1.687         73       1.687         73       1.687         73       1.687	01       2.004         88       2.128         89       1.981         59       1.981         51       1         53       1         51       1         55       1         51       1         55       1         53       1         54       1         71       1.545         73       1.647         73       1.687         73       1.687         69       1.687	01       2.004         85       2.128         80       1.981         55       1.981         67       1.981         57       1.55         71       1.545         73       1.687         18       1.687         18       1.687         63       1.687	01       2.004         88       2.128         89       1.981         59       1.981         67       1.981         51       1.981         52       1.981         63       1.1545         71       1.545         73       1.687         18       1.687         18       1.687         73       1.687         18       1.687         13       1.687         14.2       1.687         63       0.3	01       2.004         88       2.128         80       1.981         55       1.981         67       1.981         71       1.545         71       1.545         73       1.687         18       1.687         73       1.689         18       1.687         73       1.689         18       1.687         19       1.687         10       03         03       03         04       04	01       2.004         88       2.128         89       1.981         59       1.981         51       1.981         53       1.981         54       1.545         71       1.545         71       1.545         71       1.545         71       1.545         73       1.689         18       1.689         73       1.689         18       1.689         73       1.689         13       1.689         147       1.689         138       1.689         138       1.689         147       1.689         138       1.689         138       1.689         138       1.689         138       1.689         147       1.689         103       1.681	01       2.004         88       2.128         80       1.981         55       1.981         551       1         551       1         551       1         571       1.545         711       1.545         711       1.545         711       1.545         73       1.689         73       1.689         669       1.689         03       1.663         03       1.663         93       1.663	01       2.004         88       2.128         89       1.981         55       1.981         551       1         551       1         551       1         571       1.545         771       1.545         771       1.545         771       1.545         73       1.689         73       1.689         66       1.689         03       1.683         03       1.683         16       2.730	01       2.094         88       2.128         89       1.981         551       1.981         551       1.981         551       1.981         551       1.981         551       1.981         573       1.545         733       1.545         18       1.564         73       1.689         18       1.687         18       1.689         73       1.689         18       1.687         193       1.689         193       1.689         116       2.730         116       2.730	01       2.094         88       2.128         89       1.981         551       1.981         551       1.981         551       1.981         551       1.981         73       1.545         71       1.545         73       1.687         18       1.687         73       1.689         18       1.687         19       1.687         11       1.689         11       1.687         11       1.687         11       1.687         11       1.687         11       1.687         11       1.687         11       1.687         11       1.687         11       1.687         11       1.687         11       1.687         11       2.730         11       2.730	01       2.04         85       2.128         80       1.981         55       1.981         55       1.981         55       1.981         56       1.54         71       1.545         73       1.687         18       1.687         18       1.687         18       1.687         19       1.764         11       1.764         11       1.764         11       1.687         11       1.687         11       1.687         11       1.687         11       1.687         11       1.687         11       1.687         11       1.687         11       1.687         11       1.687         11       1.687         11       1.687         11       1.687         11       1.688         11       1.688         11       1.688         11       1.688         12       1.688         13       2.7730	01       2.04         85       2.128         80       1.981         55       1.981         55       1.981         55       1.981         51       1.1545         71       1.545         73       1.687         18       1.687         73       1.687         18       1.687         19       1.687         11       1.764         11       1.764         11       1.687         11       1.687         11       1.687         11       1.687         11       1.687         11       1.687         11       1.687         12       1.687         13       1.687         14       2.733         15       2.733         33       2.613	01       2.04         88       1.981         59       1.981         51       1.981         55       1.981         51       1.981         53       1.981         54       1.981         57       1.1545         71       1.545         73       1.687         188       1.687         73       1.687         188       1.687         198       1.687         118       1.687         118       1.687         118       1.687         118       1.687         118       1.687         118       1.687         118       1.687         118       1.687         118       1.687         118       1.687         118       1.687         118       1.687         118       1.687         119       2.7130         114       2.7730         1233       2.613         133       2.613	01       2.04         88       1.981         59       1.981         51       1.981         55       1.981         51       1.981         53       1.981         54       1.981         57       1.545         71       1.545         73       1.687         1.687       1.687         1.88       1.687         1.1687       1.683         1.669       1.687         1.1.687       1.687         1.687       1.687         1.687       1.687         1.687       1.687         1.687       1.687         1.687       1.687         1.693       1.687         1.693       1.687         1.693       1.687         1.6       2.718         33       2.613         33       2.613         78       1.688         1.14       2.7718         1.8       2.718         1.8       2.718         1.8       2.718	01       2.04         88       1.981         59       1.981         51       1.981         53       1.981         54       1.981         51       1.981         53       1.981         54       1.981         57       1.545         71       1.545         73       1.689         18       1.687         73       1.689         18       1.689         198       1.689         118       1.689         118       1.689         118       1.689         118       1.689         118       1.689         118       1.689         118       1.689         118       1.689         118       1.689         118       1.689         118       1.683         118       1.683         118       1.683         116       2.718         118       2.718         119       2.718         119       2.718         110       2.718         114       2.718<	01       2.004         88       2.128         80       1.981         551       1.981         551       1.981         551       1.981         551       1.981         571       1.545         711       1.545         711       1.545         711       1.545         73       1.689         18       1.689         73       1.689         16       2.718         73       1.689         16       2.718         93       1.689         16       2.718         33       2.613         33       2.613         78       00         96       1.683         16       2.718         16       2.718         16       2.718         16       2.718         17       2.718         18       2.613         10       2.718         11       2.754
$(49.84^{\circ}W)$	97.6 20		135 30	135 30 124 28	135 30 124 28 108 28	135 30 124 28 108 28 82.3 25	135     30       124     28       108     28       82.3     25       82.3     25       213     20	135         30           124         28           108         28           82.3         25           213         20           134         15	135         30           124         28           108         28           82.3         25           82.3         25           213         20           134         15           73.4         13	135         30           124         28           108         28           82.3         25           82.3         25           213         20           134         15           73.4         15           103         15	135       30         124       28         128       28         82.3       25         213       20         213       20         134       15         134       15         135       103         103       15         57.7       15	135         30           124         28           124         28           108         22           82.3         25           82.3         25           82.3         25           82.3         25           213         25           213         20           134         15           73.4         15           103         15           57.7         15           106         37	135         30           124         28           128         28           82.3         25           82.3         25           82.3         25           82.3         25           82.3         26           108         23           213         20           213         20           213         21           23.4         15           73.4         13           103         15           57.7         15           68.9         19	135         30           124         28           128         28           108         22           82.3         25           82.3         25           82.3         25           82.3         25           213         25           213         25           213         20           213         21           23.4         15           73.4         13           103         15           68.9         19           68.9         19	135       30         124       28         124       28         108       23         82.3       25         82.3       25         82.3       25         213       26         23.4       15         134       15         133       16         57.7       15         68.9       19         101       34         101       34	135       30         124       28         128       28         108       23         213       25         213       25         213       26         213       27         134       15         133       15         133       15         103       15         101       34         101       38         83.0       27	$ \begin{array}{c} 135\\ 124\\ 124\\ 108\\ 82.3\\ 213\\ 228\\ 82.3\\ 228\\ 228\\ 228\\ 23.4\\ 134\\ 134\\ 134\\ 134\\ 133\\ 155\\ 77.7\\ 135\\ 103\\ 155\\ 101\\ 34\\ 101\\ 31\\ 101\\ 31\\ 31\\ 101\\ 31\\ 31\\ 31\\ 31\\ 31\\ 31\\ 31\\ 31\\ 31\\ 3$	$ \begin{array}{c} 135\\ 124\\ 124\\ 108\\ 82.3\\ 282.3\\ 282.3\\ 282.3\\ 282.3\\ 282.3\\ 282.3\\ 273.4\\ 133.4\\ 133.4\\ 103\\ 15\\ 103\\ 15\\ 101\\ 34\\ 101\\ 316\\ 316\\ 316\\ 316\\ 316\\ 316\\ 316\\ 31$			135       135         124       282.3         128       233         108       82.3         82.3       255         23.4       15         73.4       15         73.4       15         73.4       13         106       37         15       17.6         161       34         101       34         101       34         316       37.6         40.9       44.4         417       56	$ \begin{array}{c} 135\\ 124\\ 124\\ 108\\ 82.3\\ 282.3\\ 282.3\\ 228\\ 282.3\\ 213\\ 213\\ 213\\ 213\\ 213\\ 23.4\\ 101\\ 101\\ 101\\ 101\\ 101\\ 101\\ 316\\ 83.0\\ 27.7\\ 103\\ 103\\ 316\\ 83.0\\ 217\\ 101\\ 337\\ 237\\ 237\\ 237\\ 248\\ 810\\ 348\\ 248\\ 248\\ 248\\ 248\\ 248\\ 248\\ 248\\ 2$	$ \begin{array}{c} 135\\ 124\\ 124\\ 108\\ 82.3\\ 228\\ 82.3\\ 228\\ 82.3\\ 228\\ 232\\ 232\\ 232\\ 232\\ 232\\ 103\\ 15\\ 103\\ 103\\ 103\\ 103\\ 103\\ 101\\ 101\\ 101$	$ \begin{array}{c} 135\\ 124\\ 124\\ 108\\ 82.3\\ 282.3\\ 282.3\\ 282.3\\ 213\\ 213\\ 213\\ 213\\ 213\\ 257.7\\ 103\\ 15\\ 103\\ 15\\ 103\\ 15\\ 101\\ 101\\ 101\\ 101\\ 316\\ 83.0\\ 27\\ 10\\ 101\\ 316\\ 316\\ 316\\ 327\\ 237\\ 236\\ 237\\ 236\\ 237\\ 236\\ 238\\ 238\\ 238\\ 238\\ 238\\ 238\\ 238\\ 238$	$ \begin{array}{c} 135\\ 124\\ 124\\ 108\\ 82.3\\ 228\\ 82.3\\ 228\\ 82.3\\ 228\\ 228\\ 228\\ 23.4\\ 101\\ 101\\ 101\\ 101\\ 101\\ 316\\ 83.0\\ 101\\ 101\\ 316\\ 83.0\\ 101\\ 316\\ 44.7\\ 336\\ 83.0\\ 27\\ 101\\ 3316\\ 336\\ 237\\ 236\\ 236\\ 238\\ 236\\ 238\\ 236\\ 238\\ 236\\ 238\\ 236\\ 238\\ 236\\ 238\\ 236\\ 238\\ 236\\ 238\\ 238\\ 238\\ 238\\ 238\\ 238\\ 238\\ 238$	$ \begin{array}{c} 135\\ 124\\ 128\\ 82.3\\ 82.3\\ 282.3\\ 282.3\\ 282.3\\ 282.3\\ 213\\ 213\\ 213\\ 257.7\\ 103\\ 15\\ 57.7\\ 103\\ 15\\ 57.7\\ 103\\ 15\\ 57.7\\ 101\\ 316\\ 316\\ 316\\ 316\\ 316\\ 316\\ 316\\ 31$	$ \begin{array}{c} 135\\ 124\\ 128\\ 82.3\\ 82.3\\ 82.3\\ 82.3\\ 82.3\\ 82.3\\ 108\\ 134\\ 15\\ 103\\ 15\\ 103\\ 15\\ 103\\ 15\\ 103\\ 15\\ 103\\ 15\\ 103\\ 15\\ 101\\ 101\\ 131\\ 101\\ 348\\ 83.0\\ 101\\ 101\\ 348\\ 83.0\\ 27\\ 101\\ 134\\ 101\\ 348\\ 83.0\\ 27\\ 101\\ 348\\ 83.0\\ 27\\ 101\\ 348\\ 83.0\\ 27\\ 101\\ 348\\ 83.0\\ 27\\ 27\\ 28\\ 29\\ 22\\ 28\\ 22\\ 22\\ 22\\ 22\\ 22\\ 22\\ 22\\ 22$	$ \begin{array}{c} 135\\ 124\\ 128\\ 82.3\\ 82.3\\ 82.3\\ 82.3\\ 82.3\\ 82.3\\ 108\\ 134\\ 152\\ 103\\ 15\\ 103\\ 15\\ 103\\ 15\\ 101\\ 101\\ 101\\ 101\\ 134\\ 100\\ 134\\ 83.0\\ 101\\ 101\\ 134\\ 101\\ 134\\ 101\\ 348\\ 83.0\\ 101\\ 348\\ 83.0\\ 27\\ 101\\ 134\\ 101\\ 348\\ 83.0\\ 27\\ 101\\ 134\\ 101\\ 348\\ 83.0\\ 27\\ 101\\ 348\\ 83.0\\ 27\\ 248\\ 238\\ 248\\ 228\\ 228\\ 228\\ 228\\ 228\\ 228\\ 22$	$ \begin{array}{c} 135\\ 124\\ 128\\ 108\\ 82.3\\ 82.3\\ 82.3\\ 82.3\\ 225\\ 32.3\\ 23.3\\ 108\\ 101\\ 101\\ 101\\ 101\\ 103\\ 115\\ 57.7\\ 13.4\\ 101\\ 101\\ 101\\ 13.4\\ 100\\ 133\\ 101\\ 33.6\\ 101\\ 101\\ 133\\ 101\\ 33.6\\ 101\\ 33.6\\ 101\\ 33.6\\ 101\\ 33.6\\ 101\\ 33.6\\ 101\\ 33.6\\ 101\\ 33.6\\ 101\\ 33.6\\ 101\\ 33.6\\ 101\\ 33.6\\ 101\\ 33.6\\ 101\\ 33.6\\ 101\\ 33.6\\ 101\\ 33.6\\ 101\\ 33.6\\ 101\\ 33.6\\ 102\\ 33.6\\ 102\\ 33.6\\ 102\\ 33.6\\ 102\\ 33.6\\ 102\\ 33.6\\ 102\\ 33.6\\ 102\\ 33.6\\ 103\\ 103\\ 103\\ 103\\ 103\\ 103\\ 103\\ 103$	$ \begin{array}{c} 135\\ 124\\ 128\\ 82.3\\ 82.3\\ 82.3\\ 82.3\\ 82.3\\ 82.3\\ 82.3\\ 108\\ 108\\ 101\\ 101\\ 101\\ 101\\ 101\\ 103\\ 115\\ 103\\ 115\\ 103\\ 115\\ 103\\ 115\\ 101\\ 101\\ 101\\ 103\\ 115\\ 103\\ 103\\ 103\\ 101\\ 101\\ 101\\ 101\\ 103\\ 103$	$ \begin{array}{c} 135\\ 124\\ 128\\ 82.3\\ 82.3\\ 82.3\\ 82.3\\ 82.3\\ 82.3\\ 82.3\\ 82.3\\ 82.3\\ 82.3\\ 82.3\\ 108\\ 101\\ 101\\ 101\\ 101\\ 101\\ 101\\ 101$	$ \begin{array}{c} 135\\ 124\\ 128\\ 128\\ 282.3\\ 282.3\\ 282.3\\ 282.3\\ 282.3\\ 282.3\\ 213\\ 213\\ 213\\ 282.3\\ 283.0\\ 101\\ 101\\ 101\\ 101\\ 101\\ 101\\ 101\\ 1$	$ \begin{array}{c} 135\\ 124\\ 128\\ 282.3\\ 282.3\\ 282.3\\ 282.3\\ 282.3\\ 282.3\\ 282.3\\ 282.3\\ 282.3\\ 282.3\\ 282.3\\ 282.3\\ 283.0\\ 101\\ 101\\ 101\\ 101\\ 101\\ 101\\ 101\\ 1$	$ \begin{array}{c} 135\\ 124\\ 128\\ 282.3\\ 282.3\\ 282.3\\ 282.3\\ 282.3\\ 282.3\\ 282.3\\ 282.3\\ 282.3\\ 282.3\\ 282.3\\ 282.3\\ 282.3\\ 283.0\\ 101\\ 101\\ 101\\ 101\\ 101\\ 101\\ 101\\ 1$
A (17.59°S, 14				B	B	a   a	a   a	¤   ¤	55   57   57   57   5	m   m   m   m	æ     æ   æ	שן א מין א מין א     מ   מ   מ   מ   מ	m   m   m   m   m	æ     æ     æ   æ     [   ]	m   m   m   m   m   m		שן      שן  שן  שן    שן    שן    שן    ש	8 8       8   8   8   8   8   8   9   8   8				۵.       × ۳         ۵     ۵     ۵   ۵   ۵   ۵	Q.       B B	م   م       » »       »   »   »   »   »		ﻪ   ٩   ٩	ﻪ »   ٩   ٩         ٥       ٥     ٥   ٥   ٥	¤ ¤   Q   Q       ¤	»»   Q   Q     »     »     »     »   »	¤¤  \$\\$ \$\	= = =   a       = =   =   =   =		»» @    »»	ﻪ       »¤ ٩ ٩
orea sequence	P01-02-1	1-70-I 0VII	AR01-03-1	AR01-03-1 AR01-03-1 AR01-04-1	MR01-02-1 MR01-03-1 MR01-04-1 MR01-06-2	MR01-03-1 MR01-03-1 MR01-04-1 MR02-03-1 MR02-03-1	MR01-03-1 MR01-03-1 MR01-04-1 MR02-03-1 MR02-07-1 MR02-07-1	MR01-03-1 MR01-03-1 MR01-06-2 MR02-03-1 MR02-07-1 MR03-01-1	MR01-03-1 MR01-03-1 MR01-06-2 MR02-03-1 MR02-07-1 MR02-07-1 MR03-01-1 MR04-01-1	MR01-03-1 MR01-03-1 MR01-06-2 MR02-05-1 MR02-07-1 MR02-07-1 MR03-01-1 MR04-01-1 MR04-06-1	MR01-03-1 MR01-03-1 MR01-06-2 MR02-03-1 MR02-07-1 MR03-01-1 MR04-01-1 MR04-06-1 MR05-02-1	MR01-03-1 MR01-03-1 MR01-06-2 MR02-03-1 MR02-03-1 MR02-07-1 MR03-01-1 MR03-01-1 MR04-01-1 MR05-02-1 MR06-01-2	MR01-03-1 MR01-03-1 MR01-06-2 MR02-03-1 MR02-07-1 MR02-07-1 MR02-01-1 MR03-01-1 MR04-01-1 MR06-01-2 MR06-01-2 MR06-02-1	MR01-03-1 MR01-03-1 MR01-03-1 MR02-03-1 MR02-07-1 MR02-07-1 MR02-07-1 MR04-06-1 MR06-02-1 MR06-02-1 MR06-03-1 MR06-03-1	MR01-03-1 MR01-03-1 MR01-03-1 MR02-03-1 MR02-07-1 MR02-07-1 MR02-07-1 MR03-01-1 MR05-02-1 MR06-01-2 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MR16	MR01-03-1 MR01-03-1 MR01-03-1 MR02-07-1 MR02-07-1 MR02-07-1 MR03-01-1 MR05-02-1 MR06-03-1 MR06-03-1 MR06-03-1 MR06-03-1 MR06-03-1 MR10-01-1 MR10-01-1 MR11-01-1 MR11-01-1 MR11-01-1 MR11-01-1 MR11-01-1 MR11-01-1 MR116-01-2 MR16-01-2 MR16-02-2 MR16-04-2 MR16-07-1 MR16-07-1 MR16-07-1 MR16-07-1 MR16-07-1

Table 2. (Continued.)

Table 2. ( $C\iota$	ntinuea	<i>l</i> .)																		
Sample ID	ΗT	LT	$NRM_0$	$ARM0_0$	$B_{ m  rc}/B_{ m  c}$	$M_{ m rs}/M_{ m s}$	LTD			First heating	50			S	econd heati	ng		$F_{\rm L}$	Ч	AAIC
							(per cent)	$H_{\mathrm{L}}$	$Slope_A$	$Slope_N$	$f_{\mathrm{N}}$	$r_{\rm N}$	$H_{\mathrm{L}}$	SlopeA	$Slope_{T}$	$f_{\mathrm{T}}$	$r_{\mathrm{T}}$	$(\mu T)$	$(\mu T)$	
Moorea seque.	nce $B$ ( $l$	7.50° S,	. 149.77° W	0																
MR18-07	Ш	с			1.869	0.1588	Ι					I								
MR22-07-1			82.0	251			17.4	15	1.01	0.327	0.583	0.999	0	0.992	1.01	1.00	0.999	40.0	13.1	0.5
MR23-01-2			79.4	290			12.3	15	0.522	1.25	0.661	0.998	0	1.04	0.921	1.00	766.0	10.0		
MR23-02-1	В		76.4	277	1.953	0.2008	13.8	10	0.600	0.285	0.726	0.998	0	1.02	0.994	1.00	0.999	40.0	11.4	-0.4
MR23-03-1			81.6	313	1.859	0.2019	10.7	15	0.655	0.487	0.426	0.995	0	0.981	0.959	1.00	1.00	20.0	9.74	-0.6
MR23-04-1			88.2	209	1.904	0.2686	11.5	10	0.743	0.714	0.931	0.999	0	0.985	1.02	1.00	0.999	20.0	14.3	17.2
MR23-05-1			79.8	215	1.877	0.2782	16.0	15	0.686	0.696	0.832	0.999	0	1.02	0.963	1.00	0.999	20.0	13.9	20.8
MR23-06-2			124	317	2.012	0.2650	15.0	20	0.585	1.57	0.749	0.996	0	1.02	0.979	1.00	0.999	10.0	15.7	-1.7
MR23-07-2			95.0	301	2.058	0.2722	10.7	20	0.609	0.656	0.760	0.995	0	1.02	1.00	1.00	0.999	20.0	13.1	-2.0
MR30-01-2			61.5	296			22.5	20	0.119	0.364	0.108	0.950	25	1.04	0.88I	0.803	0.998	20.0		
MR30-02-1			66.3	296	[		24.8	10	0.194	0.198	0.275	0.985	0	1.03	0.870	1.00	0.998	40.0		
MR30-03-2			43.6	319			20.6	20	0.160	0.256	0.203	0.964	15	1.02	0.847	0.917	0.995	20.0		
MR30-06-2			36.2	289			24.2	10	0.208	0.281	0.384	0.984	25	1.08	0.866	0.813	0.998	20.0		
MR30-07-1	в		45.6	307	2.096	0.1554	22.5	10	0.231	0.126	0.335	0.984	25	1.04	0.938	0.829	0.999	40.0		
MR32-01-1			104	348	1.798	0.3584	7.4	10	0.542	0.266	0.781	0.999	0	1.03	0.979	1.00	0.998	40.0	10.6	-0.4
MR32-02-1			103	382	1.951	0.3693	4.8	10	0.529	0.537	0.771	0.997	10	1.02	0.980	0.978	0.999	20.0	10.7	-1.1
MR32-03-1			111	382	1.824	0.3673	7.4	10	0.540	0.575	0.815	0.998	0	1.04	0.930	1.00	0.997	20.0		
MR32-03-2			0.69	223	1.824	0.3673	8.3	15	0.551	1.30	0.827	0.996	0	1.03	1.04	1.00	0.996	10.0	13.0	0.3
MR32-04-2			159	372	1.828	0.3252	10.7	15	0.548	1.51	0.761	0.996	0	1.01	1.01	1.00	0.999	10.0	15.1	-0.3
MR32-05-2			172	397	1.928	0.3215	13.0	15	0.502	1.68	0.734	0.999	0	0.994	1.02	1.00	0.998	10.0	16.8	0.9
MR32-06-1	в	а	121	423	2.154	0.3271	11.5	10	0.506	0.296	0.907	0.996	5	1.01	1.05	0.995	0.999	40.0	11.8	-1.5
MR32-07-2			138	361	1.812	0.3084	12.3	20	0.407	1.47	0.493	0.996	0	1.00	1.00	1.00	0.999	10.0	14.7	6.4
Tahiti sequenc	e A (17.	63° S, 1-	49.57°W)																	
PU01-01-2			132	585	1.617	0.3363	10.7	20	0.852	0.903	0.881	0.996	0	1.04	1.01	1.00	0.997	10.0	9.03	-0.7
PU01-02-1			122	570			8.3	20	0.735	0.389	0.865	0.953	0	1.03	0.993	1.00	0.998	20.0		
PU01-03-2		а	157	596	1.523	0.3647	7.4	30	0.894	1.08	0.844	0.995	0	1.07	1.03	1.00	0.996	10.0	10.8	-0.2
PU01-04-1	A	а	117	568	1.686	0.2986	17.4	15	0.673	0.454	0.895	0.996	0	1.05	0.971	1.00	0.996	20.0	9.08	-0.6
PU01-06-1			149	480	1.504	0.3736	13.8	15	0.916	0.455	0.982	0.997	0	1.03	1.05	1.00	0.999	20.0	9.10	-1.5
PU01-07-1			62.8	447			8.3	30	0.311	0.385	0.727	0.978	0	1.00	0.990	1.00	0.994	20.0		
Results are li: <sup>a</sup> Not adopted	sted from	m top te calcula	o bottom fo	r each lava flow average	sequence. N	ote that pala of the possibl	eointensities e low temper	from sp ature ox	ecimens wi	th suffix 'n' gested fron	i' are excl	uded as or T curve o	true E	the calcul.	ation of the	flow ave	rage.			
The appropriate	101 101	nmana	ATT TA TIAT	Surviv avoid	· · · · · · · · · · · · · · · · · · ·	inteend Am to	A 10W WILLIAM	vo o min	She momm	Bosica II OII	S TAT ATTA T		- 77 V -							

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Figure 3. Results of low-temperature magnetometry. Solid and broken curves indicate magnetizations and their derivatives during low-temperature cycling of 300 K SIRM, respectively (black, cooling; grey, warming). The results are grouped into five types.

#### 3.3 Hysteresis properties

Hysteresis parameters of saturation magnetization  $(M_s)$ , remanent saturation magnetization  $(M_{rs})$ , coercivity  $(B_c)$  and remanent coercivity  $(B_{rc})$  were measured for 726 small chips from selected palaeomagnetic cores. Measurements were performed on several chips for each core, three on average, by the VSM at room temperature. Core-averaged hysteresis parameters are listed in Tables 1 and 2. The Day plot (Day *et al.* 1977; Dunlop 2002) is also shown in Fig. 4.

Basically, the Day plot was empirically established for titanomagnetite solid solutions (Day *et al.* 1977). The present samples mostly fulfilled this condition (Section 3.1). One might think that some superparamagnetic contributions (e.g. Fig. 2F) would make artificial deviations in hysteresis parameters resulting in non-conformity of the Day plot. However, if theoretical mixing models such as that of Dunlop (2002) are referred to, the deviations can be used for semiquantitative estimation of the superparamagnetic contributions, and the Day plot makes sense. The hysteresis parameters seem to have been used as basic descriptors of samples in recent rock magnetic and palaeomagnetic studies. We think that the parameters determined in this study will be useful for future re-evaluation of palaeointensities.

Fig. 4 shows that data points of the present results are generally distributed between two theoretical mixing lines: SD (single domain)–MD (multidomain) and SP (superparamagnetic)–SD curves (Dunlop 2002). Remanence carriers in the measured samples are considered to consist of various grain sizes, probably an admixture of SD (and/or PSD) and MD. This is also suggested from results of reflected-light microscopy described in the next subsection.

A small number of the data points show  $M_{\rm rs}/M_{\rm s} > 0.5$ , indicating the existence of nearly equidimensional titanomagnetites governed by magnetic crystalline anisotropy. However, this may be an experimental artefact, since these data mainly come from samples with



Figure 4. Day plot (Day *et al.* 1977) for the hysteresis parameters of 726 small chips from selected palaeomagnetic cores. Some threshold values are modified following Dunlop (2002). Closed symbols indicate hysteresis parameters for which the parent cores give successful palaeointensities in the LTD-DHT Shaw experiments. Open symbols correspond to the parameters for the unsuccessful ones. It is seen that the data points generally distribute between the theoretical SD–MD and SP–SD curves of Dunlop (2002).

 $M_{\rm s}-T$  curves of type E (Tables 1 and 2), which characterizes the possible existence of a small amount of titanomaghemite. In the hysteresis measurements, a saturation field was set to be 1 T, which might not be sufficient to saturate magnetizations by Ti-poor titanomaghemites. In this case,  $M_{\rm s}$  can be underestimated. Resulting values of  $M_{\rm rs}/M_{\rm s}$  can exceed 0.5 even for samples governed by shape anisotropy.

#### 3.4 Reflected-light microscopy

Recent studies involving reflected-light microscopy have revealed that intermediate high-temperature oxidation states of titanomagnetite grains are related to erroneously high palaeointensities measured by the Thellier method (Yamamoto *et al.* 2003; Mochizuki *et al.* 2004; Oishi *et al.* 2005). Although there are some possible reasons for this relationship, it is important to examine high-temperature oxidation states in checking the quality of palaeointensity results. Therefore, we observed titanomagnetite grains in polished sections from about 50 palaeomagnetic cores.

The titanomagnetite grains in the present samples show a wide range of high-temperature oxidation states. According to the classifications by Haggerty (1991), seven stages are defined as follows:

C1: Optically homogeneous ulvöspinel-rich magnetite solid solutions (ss).

C2: Magnetite-enriched ss with a small number of 'exsolved' ilmenite lamellae parallel to {111} of the host.

C3: Ti-poor titanomagnetite ss with densely crowded 'exsolved' ilmenite lamellae parallel to {111}.

C4: The first sign of additional oxidation. Optically, an indistinct mottling of the ilmenomagnetite intergrowth is observed.

C5: Rutile and titanohaematite develop extensively within the 'exsolved' meta-ilmenite lamellae

C6: Incipient formation of pseudo-brookite (Psb) ss from rutile plus titanohaematite.

C7: Assemblage of Psb ss plus haematite ss. This is the most advanced stage of oxidation of original spinels.

Some sections show both low (C1–C2) and high (C6–C7) oxidation states (e.g. Figs 5A and D), whereas more than half of the sections contained intermediately oxidized (C3–C4) titanomagnetite grains (e.g. Figs 5B and C). According to Yamamoto *et al.* (2003), Mochizuki *et al.* (2004) and Oishi *et al.* (2005), in the Thellier experiments, samples with an intermediate high-temperature oxidation state possibly give anomalously high palaeointensities. Note that these studies employed the oxidation indices of Wilson & Watkins (1967), which are defined as six stages, I–VI. Even for such samples, they confirmed that the LTD-DHT Shaw method was applicable and yielded almost the correct values. In this context, the LTD-DHT Shaw method is preferable for determining palaeointensities from the present samples.

## 4 PALAEOINTENSITIES BY THE LTD-DHT SHAW METHOD

#### 4.1 Method

As reviewed in Yamamoto *et al.* (2003), the Shaw-type palaeointensity technique has been subject to criticism. We have therefore developed a fairly improved version of the original Shaw method (Shaw 1974), i.e. the LTD-DHT Shaw method (Tsunakawa *et al.* 1997; Yamamoto *et al.* 2003). The main procedures involved in this method are as follows (see Yamamoto *et al.* 2003, for details):

(1) A specimen is subjected to LTD. Then its memory of natural remanent magnetization (NRM) is subjected to the stepwise alternating-field (AF) demagnetization [NRM].

(2) Anhysteretic remanent magnetization (ARM) is given to the specimen and subsequently subjected to stepwise AF demagnetization [ARM00].

(3) ARM is imparted again under the same conditions as ARM00. LTD is conducted on the remanence and its memory is measured with the stepwise AF demagnetization [ARM0].

(4) The specimen is heated for acquisition of the first thermoremanent magnetization (TRM). The same procedures as in steps (1), (2) and (3) are performed for the TRM [TRM1] and ARMs [ARM10 and ARM1].

(5) The specimen is again heated for the second TRM. The same procedures as in steps (1), (2) and (3) are repeated for the TRM [TRM2] and ARMs [ARM20 and ARM2].

This method utilizes individual ARM corrections (Rolph & Shaw 1985), a double heating test (Tsunakawa & Shaw 1994) and low-temperature demagnetization. We can measure palaeointensities from SD-like remanences because the LTD treatment is known to be effective for erasing the MD-like component of Ti-poor titano-magnetites (e.g. Ozima *et al.* 1964; Heider *et al.* 1992). Borradaile *et al.* (2004) recently showed the usefulness of a LTD–AF combined demagnetization technique for isolation of a stable magnetic vector. The validity of the individual ARM corrections was experimentally assessed by Yamamoto *et al.* (2003), Pan *et al.* (2002, 2003) and Mochizuki *et al.* (2004).

The LTD-DHT Shaw method is likely to have following additional advantages:

(1) This method fits well with LTD treatment for the isolation of stable magnetization. Only six (or nine) treatments in total are required for a specimen. If similar procedures are involved in a Thellier-type experiment we have to repeat the treatment at every heating step, at least 20 times for a specimen.

(2) No laboratory CRM (chemical remanent magnetization) contaminates the NRM. This is because full demagnetization of NRM

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# (C) MP07-07

# (B) MR09-04



# (D) HH16-06





Figure 5. Representative examples of reflected-light microscopy of samples: (A) the core MR04-01, C2–C3 oxidation; (B) MR09-04, C4–C5; (C) MP07-07, C4–C7; (D) HH16-06, C7. These classifications follow Haggerty (1991).

is done prior to the first laboratory heating which produces 'TRM1'. This certifies the fidelity of the palaeodirection if LTD and AF demagnetization can remove secondary components. In Thellier-type experiments, NRM is often contaminated by CRM during progressive laboratory heating (e.g. Mochizuki *et al.* 2004).

(3) The laboratory heating process is thought to be analogous to a natural process (Oishi *et al.* 2005). In contrast to progressive heating in Thellier-type experiments, samples are directly heated above the Curie temperature and cooled down to room temperature.

(4) One of two endpoints for linear segments in NRM–TRM1\* diagrams is fixed to steps of maximum AF (TRM1\* being the corrected TRM1). This reduces ambiguities in the calculation of palaeointensity. Both endpoints of the linear segments in Arai diagrams are selectable, which allows for more ambiguity in Thellier-type experiments.

(5) A series of measurements can be easily automated since the procedures of the LTD-DHT Shaw method mainly consist of progressive AF demagnetizations. We use an automated spinner magnetometer with an AF demagnetizer (Natsuhara-Giken Dspin-2; Kono *et al.* 1984, 1997). A SQUID magnetometer equipped with an automated AF demagnetizer is also available.

#### 4.2 Experiments and data analysis

In the present study, a total of 361 specimens were used in LTD-DHT Shaw experiments. They were heated in a vacuum (10-10<sup>2</sup> Pa) at a top temperature of 610 °C for 20 and 30 min (first and second heatings, respectively). Laboratory TRM was imparted in a 5.0–50.0  $\mu$ T DC field while ARM was imparted in a 100  $\mu$ T field. Progressive AF demagnetization was performed at 5–10 mT intervals up to 160 mT. In the LTD treatment, specimens were soaked in liquid nitrogen in a plastic Dewar for 10 min and then kept outside at room temperature for an hour. This cycle was performed in a magnetically shielded case where the residual field was less than 100 nT. All remanences were measured with an automated spinner magnetometer (Natsuhara-Giken Dspin-2).

For constructions of NRM–TRM1\* and TRM1–TRM2\* diagrams, TRMs were corrected with the technique of Rolph & Shaw (1985) (corrected TRMs being denoted TRM1\* and TRM2\*, respectively). This correction is based on the assumption that changes in the TRM coercivity spectra can be followed by those of ARM.

Similar to the previous studies by Yamamoto *et al.* (2003), Mochizuki *et al.* (2004) and Oishi *et al.* (2005), the results are judged by the following quantitative selection criteria:

(1) The primary component is recognized in the Zijderveld diagram.

(2) There should be a linear portion in the NRM–TRM1\* diagram. This should not be less than 15 per cent of the original NRM intensity ( $f_N \ge 0.15$ ), and its correlation coefficient should be larger than 0.995 ( $r_N \ge 0.995$ ).

(3) The linear portion ( $f_T \ge 0.15$  and  $r_T \ge 0.995$ ) also should exist in the TRM1–TRM2\* diagram. Its slope is unity within experimental error ( $1.05 \ge \text{Slope}_T \ge 0.95$ ).

(4) Both linear portions should include the maximum AF demagnetization steps.

Criterion (4) is implicitly involved in the previous studies. A schematic view of the data analysis is illustrated in Fig. 6.



Figure 6. Schematic view of the data analyses for the LTD-DHT Shaw experiments. These figures illustrate example calculations for the results of (A) HH09-04-1 and (B) BR15-05-1 with Types A and B thermomagnetic curves, respectively. Refer to Yamamoto *et al.* (2003) for detailed experimental procedures. Note that the remanences shown in these figures are values after vectorial subtraction of the remanences at 160 mT (maximum AF step). Thus, values of NRM<sub>0</sub> indicated in these figures do not necessarily correspond to those in Tables 1 and 2.

## 4.3 Results

Comparing magnitudes of ARM0 before and after the LTD treatment, we can roughly estimate the MD contributions for the present samples. Fig. 7 shows a distribution of the LT-demagnetized fractions in ARM0. Since most samples exhibit 0–20 per cent loss of ARM0, the MD contribution should not cause serious problems in the palaeointensity experiments. However, 25 specimens show more than 20 per cent loss up to 31.5 per cent by the LTD treatment, resulting in the effective removals of undesirable remanences.

Applying the quantitative selection criteria described in the previous subsection, we obtained 195 successful results (a success rate of 54 per cent). Representative results are shown in Fig. 8. The remaining 166 results were rejected, mainly because (1) linear



Figure 6. (Continued.)

portions were not detected in the NRM–TRM1\* diagrams ( $r_{\rm N} < 0.995$ ; e.g. Figs 9A and C) and (2) slopes of linear portions in the TRM1–TRM2\* diagrams were not unity (Slope<sub>T</sub> < 0.95 or 1.05 < Slope<sub>T</sub>; e.g. Figs 9A and B). These results are summarized in Tables 1 and 2.

The successful results exhibit good linearity in both NRM– TRM1\* and TRM1–TRM2\* diagrams (Fig. 8). As most of their linear portions are associated with  $f_{\rm N} \ge 0.30$  and  $f_{\rm T} \ge 0.90$ (Fig. 10), those palaeointensities are obtained from relatively large fractions of the original NRMs and the ARM correction is fairly applicable for laboratory TRMs. The obtained palaeointensities are thought not to be systematically influenced by the ARM correction because there is no obvious correlation between the measured palaeointensities and the slopes in the corresponding ARM0–ARM1 diagrams (Fig. 11A). The palaeointensities are also independent of the hysteresis properties (Figs 11B and C), suggesting no effect of grain size of magnetic minerals on the present results.



**Figure 7.** A histogram of LT-demagnetized fractions in ARM0 for the LTD-DHT Shaw experiments. The demagnetized ratios are expressed as remanence decrease after LTD to the original.

A noticeable feature in the present results is that samples collected from site PU06 show similar failures in the LTD-DHT Shaw experiments. Zijderveld diagrams clearly showed the existence of a single component, and TRM1-TRM2\* diagrams guaranteed reproducible laboratory TRMs. Slopes of unity in ARM0-ARM1 diagrams indicate little occurrence of laboratory alteration in remanence carriers. In spite of these favourable features, all NRM-TRM diagrams showed convexity (e.g. Fig. 9C). These facts suggest that NRMs of PU06 may not have entirely originated from thermoremanent magnetizations. Other types of remanence, like thermochemical remanent magnetization (TCRM), were possible 'contaminants' during initial cooling in nature (e.g. Yamamoto et al. 2003). Indeed, sister specimens subjected to Thellier experiments gave two-sloped Arai diagrams (see Figs 18J and K). This evidence implies that the LTD-DHT Shaw method offers a possible way to discriminate natural TCRM, as suggested by Yamamoto et al. (2003). An interesting fact observed in these PU06 specimens is that there are many pseudobrookite grains (C6-C7 oxidation, e.g. Fig. 12A). The existence of pseudo-brookites has been believed to validate true TRM (Dunlop & Özdemir 1997), but the present study yields an exceptional case. Since C4-class oxidation grains simultaneously occur in the PU06 specimens (e.g. Fig. 12B), they might be a source of the non-ideal behaviour in both the LTD-DHT Shaw and Thellier experiments.

## 5 PALAEOINTENSITIES BY THE THELLIER METHOD

### 5.1 Experiments and data analysis

Coe's version of the Thellier method (Coe 1967) was applied to 40 specimens of good thermal stability (Types A and B in Section 3.1; Fig. 2). These results can be compared with the companion LTD-DHT Shaw results because their sister specimens have already given successful palaeointensity results in the LTD-DHT Shaw experiments.

In the Thellier experiments, the specimens were subjected to a series of zero-field and in-field heating cycles at 20–50 °C inter-

vals up to 600 °C. Partial TRM checks were conducted at every other temperature step. Above 200 °C, at least one pTRM-tail check (Riisager & Riisager 2001) step was involved for every 100 °C interval, that is, at least five pTRM-tail checks for each specimen. This check detects a vectorial difference between the pTRM tail of laboratory-produced pTRM and the pTRM tail that is embedded in TRM (e.g. Shcherbakova *et al.* 2000; Riisager *et al.* 2004). The heating cycle was done in air for 1–1.5 hr with a TDS-1 (Natsuhara-Giken) or MMTD-18 (Magnetic Measurements) electric furnace. TRM was imparted in a DC field of 15.0–30.0  $\mu$ T, which was applied throughout the in-field cycles. All remanent magnetizations were measured by a SMM-85 or ASPIN (Natsuhara-Giken) spinner magnetometer with a resolution better than  $\pm 10^{-8}$  A m<sup>2</sup>.

Although selection criteria for the Thellier experiments differ in previous studies, we adopted the following:

(1) A stable primary component is recognized in the Zijderveld diagram of zero-field step data (NRM).

(2) A linear portion should be recognized in the Arai diagram. It is composed of the primary component and is not less than 15 per cent of the original NRM ( $f \ge 0.15$ ). This portion should have four or more data points ( $N \ge 4$ ).

(3) The linear portion should exhibit positive pTRM checks. This is judged by an agreement between reproduced pTRM and first TRM at the  $2\sigma$  level. The error ( $\sigma_{pTRM}$ ) is evaluated from experimental uncertainties of remanence measurements ( $\sigma_{meas}$ ), heating temperatures ( $\sigma_{temp}$ ) and applied DC fields ( $\sigma_{DC}$ ), i.e.  $\sigma_{pTRM}^2 = \sigma_{meas}^2 + \sigma_{temp}^2 + \sigma_{DC}^2$ .

For the pTRM tail checks, accordance between the first and repeated zero-field data was examined at the  $2\sigma$  level. However, their use-fulness is still under debate (e.g. Biggin & Thomas 2003a). Yu *et al.* (2004) showed that a proper pTRM tail check could be made only when a laboratory field was twice as large as an ancient field and was applied parallel to a NRM direction. A laboratory field perpendicular to the NRM results in an overestimated pTRM tail, while a field antiparallel to the NRM causes underestimation. We do not incorporate the results of the pTRM tail checks in the selection criteria.

#### 5.2 Results and discussions

Successful results were obtained for 18 specimens (Table 3). Fifteen results showed quality factors q (Coe *et al.* 1978) of more than 5.0, indicating good Thellier results. The successful results can be classified into following three types.

The first type is characterized by Arai diagrams with a single slope (Figs 13A and B). This type is observed for four specimens, TA15-01-2, MR14-03-2, PU01-03-4 and PU01-06-2. Although the Arai diagram of TA15-01-2 (Fig. 13B) appears to be two-segmented, the low blocking temperature range is probably contaminated by secondary magnetization. These palaeointensities are generally consistent with those of the sister specimens by the LTD-DHT Shaw method.

A feature of the second type of result, from 11 specimens, is two segments in the Arai diagrams (Fig. 13C). Slopes of the low blocking temperature ( $T_{\rm B}$ ) portion gave high palaeointensities whereas those of the high  $T_{\rm B}$  yielded low palaeointensities. The differences in palaeointensities between the two segments are up to about eight times (187 and 22.9  $\mu$ T in HH16-03-2). It is noted that palaeointensities from the high  $T_{\rm B}$  portion are not far from the LTD-DHT Shaw palaeointensities of the sister specimens.

Three specimens resulted in the third type of result, where only a single slope is seen in the Arai diagrams. They show incompatible



**Figure 8.** Representative successful results in the LTD-DHT Shaw experiments. (A) PU01-03-2 from Tahiti. (B) TA15-01-1 from Tahaa. (C) HH16-06-1 and (D) HH09-04-1 from Huahine. The left three diagrams indicate results from the first laboratory heating while the right ones are from the second heating. Linear portions consist of closed symbols. Zijderveld diagrams are also shown as insets, where closed and open symbols indicate projections onto horizontal and vertical planes, respectively (squares are NRM before LTD). Units are  $10^{-5}$  A m<sup>2</sup> kg<sup>-1</sup>. The Thellier results for the sister specimens are shown in Fig. 13.

palaeointensity with the companion LTD-DHT Shaw results. However, if we take alternative slopes in the high  $T_{\rm B}$  portions (e.g. the dotted line in Fig. 13D) with insufficient data points (N = 3) they give apparent palaeointensities consistent with the LTD-DHT Shaw results.

In summary, the present Thellier experiments mainly exhibit twosloped Arai diagrams, which are a possible cause of overestimated palaeointensities (e.g. Yamamoto *et al.* 2003). Overestimations by the Thellier method may also be suggested from the hysteresis parameters of the core-averaged values for the specimens used for palaeointensity determination in the Thellier experiments (Fig. 14). It is obvious that the data points in the Day plot are distributed close to the mixing lines between the SD and MD of Dunlop (2002). Oishi *et al.* (2005) suggest that samples with data points close to SD–MD



Figure 8. (Continued.)

mixing lines tend to give erroneously high palaeointensities by the Thellier method.

However, routine application of the above criteria could not filter out the erroneous results. Anomalously high palaeointensities may be observed especially from the low  $T_{\rm B}$  portion of the second type. A stringent criterion of  $q \ge 5.0$ , which is often adopted (e.g. Mochizuki *et al.* 2004), could not reject very high palaeointensities (e.g. 145  $\mu$ T in HH16-06-3 and 167  $\mu$ T in PU06-04-3). Although the best way to avoid contamination of such anomalous data is probably to discard all the two-segmented results (e.g. Valet 2003), this procedure results in the loss of a large number of the present palaeointensity estimations. Only four results of the first type remain. There is another criterion of  $f \ge 0.50$  suggested by Biggin & Thomas (2003a). If we add this criterion, 13 results survive. These palaeointensities, except for BR15-02-2 and HH09-04-2, seem to be improved (closed circles in Fig. 15). Even for BR15-02-2 and HH09-04-2, if their alternative segments of high  $T_{\rm B}$  (discarded due to f < 0.50) are adopted, they also become closer to the LTD-DHT Shaw results (open circles in Fig. 15). Discrepancies between the Thellier and the LTD-DHT Shaw data are up to about 40 per cent, which is similar to the results



Figure 9. Examples of rejected results in the LTD-DHT Shaw experiments. (A) MR16-05-2 from Moorea. (B) PU05-11-1 and (C) PU06-04-1 from Tahiti. These do not pass the quantitative selection criteria because of (A) a low correlation coefficient ( $r_N = 0.984$ ) in the first heating as well as a non-unity slope (Slope<sub>T</sub> = 1.21) in the second heating and (C) a low correlation coefficient ( $r_N = 0.936$ ) in the first heating.

found for historical lavas by Yamamoto *et al.* (2003), Mochizuki *et al.* (2004) and Oishi *et al.* (2005).

6 EVALUATION OF THE LTD-DHT SHAW PALAEOINTENSITIES

We have obtained 195 successful LTD-DHT Shaw palaeointensities using the quantitative selection criteria (Section 4.3). These criteria seem to be able to reject a majority of the undesirable results, but the reliability of the selected results will be further examined from several aspects.

## 6.1 Low-temperature oxidation

As discussed in Section 3.1, some samples possibly suffered from low-temperature oxidation. They might give biased



Figure 10. Histograms of (A) NRM fractions ( $f_N$ ) and (B) TRM fractions ( $f_T$ ) for the successful LTD-DHT Shaw results.

palaeointensities. Although the thermomagnetic experiments suggest low degrees of low-temperature oxidation (e.g. Fig. 2E), for safety's sake we do not use the 31 palaeointensities from seven flow units (MP19, BR02, HH05, HH06, HH08, HH12, and MP12) in calculations of flow averages.

#### 6.2 Applicability of the ARM correction

Samples from sites BR10 and BR16 show curved NRM–TRM1\* diagrams, high  $B_c$  portions of which pass the quantitative selection criteria (e.g. Fig. 16). As their Zijderveld diagrams suggested single primary components, their curvature could not be caused by secondary magnetization. For example, in Fig. 16, a NRM–TRM diagram obviously shows a downward concave feature for  $B_c \ge 10$  mT (which is sufficient to remove a secondary magnetization), but the corresponding portion in a ARM0–ARM1 diagram gives nearly a straight line. This suggests that ARM changes in the first laboratory heating may not follow TRM changes for some samples. Pan *et al.* (2003) observed similar NRM–TRM\* diagrams from samples

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with heavy laboratory alterations (e.g. C20 in Fig. 1 of Pan *et al.* 2003). If we adopt a possible linear segment from sample C20 in Pan *et al.* (2003), it gives 30 per cent lower palaeointensity than the true field value (50  $\mu$ T). Therefore, the palaeointensities obtained from sites BR10 and BR16 might be biased, although our specimens did not seem to suffer from such alterations. These nine results are temporarily not used for calculations of flow averages.

# 6.3 Upward convex features in the NRM-TRM1\* diagrams

A number of the successful LTD-DHT Shaw results show some convexity in the NRM–TRM1\* diagrams. An evaluation of the convexity is vague regarding the criterion of correlation coefficients. For example, TA15-01-1 and HH09-04-1 passed the criterion, but their high  $B_c$  intervals in the NRM–TRM1\* diagrams exhibited upward convex features (Figs 8B and C). In the usual Thellier experiments, downward concave features are often observed in Arai diagrams, and there is growing consensus that the palaeofield should not be



Figure 11. Relation between the LTD-DHT Shaw palaeointensities and (A) slopes in the ARM0–ARM1 diagrams (Slope<sub>A</sub> in the first heating), (B) ratios of remanent saturation magnetization to saturation magnetization ( $M_{\rm rs}/M_{\rm s}$ ) and (C) ratios of remanent coercivity to coercivity ( $H_{\rm rc}/H_{\rm c}$ ). Correlation coefficients (r, absolute values) are shown in each diagram.



Figure 12. Reflected-light microscopy for the palaeomagnetic core of PU06-04: (A) C7-class oxidation grain, (B) C4-class oxidation grain.

estimated using such diagrams (e.g. Valet 2003). We may apply similar cautions to the present LTD-DHT Shaw results.

#### 6.3.1 Introduction of the Akaike information criterion (AIC)

One of the ways to evaluate the convexity is to introduce the Akaike information criterion (AIC; Akaike 1980). This allows statistical estimation of an optimal model from candidates by a trade-off between goodness of fit data and a number of parameters. The smaller the value of the AIC, the better the model is. If a linear and a quadratic polynomial are introduced as regression functions for the NRM–TRM1\* diagrams, their AICs are defined as follows:

AIC1 = 
$$N \times \left( \ln 2\pi + 1 + \ln \frac{\chi_1^2}{N} \right) + 2 \times (1+2),$$
 (1)

AIC2 = 
$$N \times \left( \ln 2\pi + 1 + \ln \frac{\chi_2^2}{N} \right) + 2 \times (2+2),$$
 (2)

where *N* is the number of data points and  $\chi_1$  and  $\chi_2$  are residuals of the linear and the quadratic fit for the NRM–TRM1\* diagrams, respectively. Thus, a difference in the AIC between the linear and quadratic fits ( $\Delta$ AIC) is

$$\Delta \text{AIC} = \text{AIC1} - \text{AIC2} = N \times \ln \frac{\chi_1^2}{\chi_2^2} - 2.$$
(3)

If  $\Delta AIC \leq 1$ , the quadratic fitting is statistically not better than the linear one, suggesting no convexity in the diagram.  $\Delta AICs$  are calculated for all the NRM–TRM1\* diagrams of the successful results (195 specimens). They are listed in Tables 1 and 2, and their distribution is illustrated in Fig. 17. Sixty-nine results show  $\Delta AIC \leq 1.0$ , indicating that the quadratic fit is not preferred. The other results

seem to prefer the quadratic fit. For instance,  $\triangle$ AICs of TA15-01-1 and HH09-04-1 were 18.5 and 11.9 (Fig. 8B and C). As stated before, their NRM–TRM1\* diagrams appeared to be upward convex especially for the high- $B_c$  portions. On the other hand, PU01-03-2 yielded  $\triangle$ AIC of -0.2 for its NRM–TRM1\* diagram without obvious convexity (Fig. 8A). Possible causes of the convexity are discussed in the following section.

#### 6.3.2 LTD-Thellier experiments

The convexity observed in the NRM-TRM1\* diagrams may be analogous to concavity in the Arai diagrams often reported from the usual Thellier experiments. Since LTD-DHT Shaw results cannot be directly compared with Thellier results because of the LTD treatment, we further conducted LTD-Thellier experiments (e.g. Yamamoto et al. 2003) on four specimens (MP05-05-3L, MP07-07-3L, HH09-07-4L and PU06-04-4L). All of their sister specimens had already given palaeointensities using the Coe (1967) version of the Thellier method (MP05-05-2, MP07-07-2, HH09-07-3 and PU06-04-3). The LTD-DHT Shaw experiments yielded three successful palaeointensities (MP05-05-1, MP07-07-1 and HH09-07-2). PU06-04-1, which is the sister specimen of PU06-04-4L, unfortunately did not pass the criteria. Fig. 18 illustrates all the results obtained using the Coe (1967) version of the Thellier method with and without LTD, and by the LTD-DHT Shaw method. Noticeable features in these diagrams are that all the Thellier results show two-segmented Arai diagrams (Figs 18B, E, H and K), and also that the LTD-DHT Shaw results give large  $\triangle$ AICs (45.1, 53.5 and 13.4; Figs 18C, F and I).

In the LTD-Thellier experiments, all the specimens were chilled in liquid nitrogen for 10 min after each of the progressive zero-field

 Table 3. Experimental results with the Thellier method.

Sample ID	NRM <sub>0</sub>	PTRM	$T_1 - T_2$	N	r	q	f	Slope	$F_{\rm L}$	F	PTRM tail
									$(\mu T)$	$(\mu T)$	
MP02-06-2	361	20-300							15.0		
MP05-05-2	241	20-600	400-500	5	0.989	1.94	0.231	$1.48 \pm 0.13$	25.0	37.0 <sup>a</sup>	+
			475-540	4	0.999	9.18	0.536	$0.839\pm0.031$	25.0	21.0	+
MP06-05-2	277	20-600	300-475	7	0.996	6.97	0.348	$2.80\pm0.12$	25.0	70.0 <sup>a</sup>	+
			500-580	5	0.999	14.7	0.599	$0.925 \pm 0.028$	25.0	23.1	+
MP07-07-2	296	20-600	300-475	5	0.982	2.82	0.291	$3.18 \pm 0.27$ $1.05 \pm 0.05$	25.0	79.6ª 26.1	+
MP12-07-3	134	20-200			0.770		0.040	1.05 ± 0.05	15.0	20.1	- -
DD04.05.2	222	20-200							15.0		
BR04-05-2	223	20-200	150 450		0.095	5.01	0.502	1.07 + 0.14	15.0	20.2	_
BK13-02-2	00.0	20-300	350-475	8 5	0.985	2.21	0.302	$1.97 \pm 0.14$ $1.23 \pm 0.13$	15.0	29.2 18.5 <sup>a</sup>	_
BR15-05-4	108	20-520	335-425	4	0.989	1.48	0.232	$1.94 \pm 0.20$	20.0	38.8 <sup>a</sup>	+
			425-500	4	0.983	1.31	0.256	$0.733\pm0.096$	20.0	14.7 <sup>a</sup>	_
BR15-07-2	98.1	20-475		_	—	—	—		15.0		_
BR18-02-3	345	20-520			—	—	—		15.0		—
TA08-06-3	396	20-200			_	_	_	_	15.0		_
TA11-05-3	423	20-200			_	_	_		15.0		_
TA15-01-2	86.4	20-600	500-600	5	0.998	16.2	0.774	$0.448 \pm 0.016$	15.0	6.72	+
TA15-06-2	94.2	20-520			_	_	_		15.0	_	_
TA16-04-2	78.6	20-300						—	30.0		_
TA16-07-2	28.6	20-600		_	—	_	_		15.0	_	—
HH09-04-2	328	20-560	300-520 <i>520-560</i>	9 3	0.992 <i>0.993</i>	9.55 1.84	0.510 <i>0.430</i>	$\begin{array}{c} 2.53 \pm 0.12 \\ 0.609 \pm 0.071 \end{array}$	30.0 <i>30.0</i>	75.9 18.3 <sup>a</sup>	++++
НН09-07-3	357	20-600	250-500 500-575	8	0.991	6.10 4.41	0.405	$5.74 \pm 0.32$ 1 53 ± 0 14	15.0	86.1 <sup>a</sup>	+
HH16-03-2	409	20-600	100-475	10	0.956	3.93	0.481	$12.4 \pm 1.3$	15.0	187 <sup>a</sup>	_
			475-600	6	0.995	12.8	0.824	$1.53 \pm 0.08$	15.0	22.9	+
HH16-06-3	443	20-560	100-450	10	0.986	6.81	0.456	$4.82\pm0.28$	30.0	145 <sup>a</sup>	+
			450-560	6	0.995	10.5	0.687	$0.971 \pm 0.049$	30.0	29.1	+
HH20-06-3	599	20-370							20.0		_
MR01-02-2	97.8	20-520	335-475 475-520	6	0.992	4.18	0.329	$1.85 \pm 0.12$ 0.705 + 0.047	20.0	36.9 <sup>a</sup>	+
MR01-03-2	101	20-300						0.705 ± 0.047	15.0		
MR01-07-3	84.5	20-425							15.0		_
MR02-03-2	89.2	20-520	200-425	7	0.995	4.79	0.270	$1.42 \pm 0.07$	25.0	35.5 <sup>a</sup>	+
			450-520	4	0.995	2.24	0.244	$0.512\pm0.037$	25.0	12.8 <sup>a</sup>	+
MR04-01-2	56.7	20-520	335-475	6	0.998	7.92	0.316	$0.773 \pm 0.025$	25.0	19.3 <sup>a</sup>	+
MD0( 01 2	967	20,520	4/5-520	3	0.999	1.61	0.1//	$0.445 \pm 0.024$	25.0	11.1 <sup>ª</sup>	+
MR06-01-3	80./	20-520	_	_	_	_	_	_	20.0		_
MR00-00-3	3/.3 300	20-520	370 475		0.004	2.61	0 222	$1.56 \pm 0.10$	15.0	38 Qa	
WIK09-04-2	500	20-000	475-560	5	0.999	11.2	0.222	$0.690 \pm 0.020$	25.0	17.3 <sup>a</sup>	+
MR12-01-2	142	20-475							15.0		_
MR14-03-2	306	20-600	400-520	6	0.999	17.2	0.560	$0.948 \pm 0.021$	25.0	23.7	+
MR23-02-3	58.6	20-520			_	_	_	_	15.0		_
MR23-03-2	36.4	20-300			—	_	—		20.0		—
MR32-02-3	122	20-300			—	—	—	—	15.0		_
MR32-06-2	127	20-300			—	—	—		15.0		—
PU01-03-4	149	20-500	300-500	7	0.998	21.6	0.822	$0.752\pm0.023$	15.0	11.3	_
PU01-06-2	136	20-520	400-520	6	0.997	15.2	0.744	$0.513\pm0.019$	20.0	10.3	_
PU01-07-3	45.9	20-370							15.0		—
PU06-04-3	547	20-600	300-500	8	0.995	8.22	0.378	$6.68 \pm 0.26$	25.0	167 <sup>a</sup>	+
TD02 04 2	116	20.200	520-580	4	0.999	15.2	0.597	$2.03 \pm 0.05$	25.0	50.9	+
1 KUZ-U4-3	110	20-300							23.0		

NRM<sub>0</sub>, initial NRM intensity; PTRM, acceptable temperature interval in the pTRM test;  $T_1 - T_2$ , N, r, q, f, slope, temperature interval, number of data points, correlation coefficient, quality factor, NRM fraction, and slope of the linear NRM–TRM portion in the Arai diagram;  $F_L$ , laboratory-induced DC field for TRM; F, calculated palaeointensity; PTRM tail, positive (+) or negative (-) pTRM tail check for the linear segment. Note that data line indicated in italic is a reference (see text).

<sup>a</sup>Rejected if the criterion of  $f \ge 0.50$  is adopted.

and in-field heatings. The LTD treatment was done in a magnetically shielded case and the memories were measured. Except for these points, the experimental procedures were the same as in Section 5.1. We can thus construct Arai diagrams for LT-surviving NRM and TRM components (Figs 18A, D, G and J). The results are examined with the same selection criteria as in Section 5.1, and are listed in Table 4.

As indicated in the Zijderveld diagrams (insets in Fig. 18), LTdemagnetized components are not very large in the present specimens. However, in comparison with the non-LTD-Thellier results,



Figure 13. Representative successful results in the Thellier experiments. Linear portions consist of closed circles. Positive and negative pTRM-tail checks are indicated by closed and open diamonds, respectively. Zijderveld diagrams are also shown as insets. The results could be classified into three types: (A) and (B) single-slope type, (C) two-segmented type and (D) quasi two-segmented type. Units are  $10^{-5}$  A m<sup>2</sup> kg<sup>-1</sup>.

the two-segmented features in the Arai diagrams for the LTD-Thellier results are clearer. This is analogous to the results for the Kilauea, Hawaii, 1960 lava (Yamamoto et al. 2003). In their experiments, samples with low and intermediate levels of hightemperature oxidation (corresponding to C1-C3 and C2-C4 oxidations; A-4-4L and B-9-4L in Yamamoto et al. 2003) exhibited more concave Arai diagrams in the LTD-Thellier experiments than in the non-LTD-Thellier ones (Figs 5d and e in Yamamoto et al. 2003). Although the reason for such a phenomenon is still controversial, they might be evoked by acquisition of thermochemical remanent magnetization (TCRM) during natural cooling of the lava, as suggested by Yamamoto et al. (2003). TCRM is contaminated into NRM and it is carried by a number of small domains of Ti-poor titanomagnetites, which are products of moderate high-temperature oxidation and are thought to consist partly of SD-like remanences. It is difficult to regard MD contribution as a main cause because most MD remanences are thought to be erased by LTD treatment.

For specimens of MP05-05-3L and MP07-07-3L, their low  $T_{\rm B}$  (43.0 and 59.8  $\mu$ T) and high  $T_{\rm B}$  palaeointensities (20.5 and 20.1  $\mu$ T) are respectively larger and smaller than the corresponding LTD-DHT Shaw palaeointensities (33.4  $\mu$ T for MP05-05-1 and 35.0  $\mu$ T for MP07-07-1). This suggests that the LTD-DHT Shaw palaeointensities obtained from the upward convex NRM-TRM1\* diagrams can be weighted-averaged values of the low and high  $T_{\rm B}$ LTD-Thellier palaeointensities. PU06-04-4L exhibited a large difference between the low  $T_{\rm B}$  (161  $\mu$ T) and high  $T_{\rm B}$  palaeointensities (43.7  $\mu$ T). PU06-04-1 did not yield a successful palaeointensity in the LTD-DHT Shaw experiment because its NRM-TRM1\* diagram showed an excessive upward convexity giving  $r_N < 0.995$  for a linear fit. It is possible that the difference between the two palaeointensities is so large that their mixture results in excessive convexity in the NRM–TRM1\* diagram. HH09-07-4L gave a consistently high  $T_{\rm B}$ LTD-Thellier palaeointensity (18.3  $\mu$ T) with the LTD-DHT Shaw result (17.2 µT).



**Figure 14.** Day plot of the core-averaged hysteresis parameters for the specimens giving palaeointensities in the Thellier experiments. Open and closed symbols indicate the single-slope and two-segmented types, respectively. The parameters are referred from Tables 1 and 2. It is obvious that data points distribute along the mixing lines between SD and MD of Dunlop (2002). This kind of trend is warned against by Oishi *et al.* (2005).



**Figure 15.** Comparison between the Thellier and the LTD-DHT Shaw palaeointensities for the sister specimens. The vertical axis indicates the normalized Thellier palaeointensity (by the LTD-DHT Shaw palaeointensity) while the horizontal one is the individual site. Closed symbols are the results satisfying the quantitative selection criteria with  $f \ge 0.50$ . Open symbols are the alternative results (see text).

## 6.3.3 Threshold $\triangle AIC$ for data selections

The above discussions suggest that the LTD-DHT Shaw palaeointensities accompanied by large  $\triangle$ AICs may have equivalent qualities to Thellier palaeointensities with concave Arai diagrams. According to the growing consensus on analysis of Thellier results, it seems better not to adopt such LTD-DHT Shaw palaeointensities for further discussions. It is, however, difficult to define an exact threshold value of  $\triangle$ AIC at which results should be discarded. In this study, we temporarily determined the threshold value for the present data set based on several concrete examples. In this section, four LTD-Thellier results were obtained. Three of them were accompanied with the companion LTD-DHT Shaw results. MP05-05-1 and MP07-07-1 gave  $\Delta AICs$  of 45.1 and 53.5. As discussed before, these LTD-DHT Shaw results are considered to be weighted-averages of the corresponding low and high  $T_{\rm B}$  LTD-Thellier results. On the other hand, HH09-07-2 resulted in  $\Delta AIC$  of 13.4, and its LTD-DHT Shaw palaeointensity (17.2  $\mu$ T) is consistent with the companion high  $T_{\rm B}$  LTD-Thellier palaeointensity (18.3  $\mu$ T, HH09-07-4L).

In Sections 4.3 and 5.2 we can find four pairs of LTD-DHT Shaw and usual Thellier results. Although simple comparison between both results is not straightforward due to a lack of LTD treatment in the usual Thellier results, it may reinforce our ideas. There are three LTD-DHT Shaw results showing relatively large  $\Delta$ AICs. TA15-01-1 gave  $\Delta$ AIC of 18.5. The LTD-DHT Shaw palaeointensity (7.68  $\mu$ T) is concordant with the companion Thellier one (6.72  $\mu$ T, TA15-01-2). Also, HH16-06-1 and HH09-04-1 yielded  $\Delta$ AICs of 7.2 and 11.9. Their LTD-DHT Shaw results (29.6 and 18.2  $\mu$ T) agree well with the companion high  $T_{\rm B}$  Thellier palaeointensities (29.1 and 18.3  $\mu$ T; note that the latter is the reference, see Section 5.2).

If the agreements between the LTD-DHT Shaw and the high  $T_{\rm B}$ Thellier palaeointensities are tentatively permitted when the Thellier experiments yield two-sloped Arai diagrams, the quality of the LTD-DHT Shaw palaeointensities with  $\Delta AIC \leq 18.5$  does not seem to be too bad. Therefore, we temporarily take a threshold  $\Delta AIC$  of 15, which is set to be slightly on the safe side.  $\Delta AIC$  exceeding ~15 is possibly a sign of an undesirable LTD-DHT Shaw palaeointensity. There are 49 results with  $\Delta AIC > 15$  among the present successful results (Fig. 17). It is, however, emphasized that this threshold is limited to the present data set.

# 7 GEOMAGNETIC FIELD INTENSITY DURING THE LAST 5 MYR

# 7.1 New data set from the LTD-DHT Shaw palaeointensities

Discussions in Sections 6.1 and 6.2 discriminated 151 LTD-DHT Shaw palaeointensities. Their statistical results are summarized in Table 5. In this table it is noted that site means of RT12, RT18 and HH11 are calculated excluding four outliers because they are statistically distinguishable from the site means at the  $2\sigma$  level. Yamamoto *et al.* (2003) observed the same phenomena from the Kilauea, Hawaii, 1960 lava, and obtained a true palaeointensity after excluding outliers.

From these data, we can choose 24 reliable site-mean LTD-DHT Shaw palaeointensities by the following criteria:

(1) Each mean is determined from no fewer than three individual results ( $N \ge 3$ ).

(2) The standard deviation is within 20 per cent ( $\sigma \leq 20$  per cent).

(3) The minimum value of  $\triangle$ AIC among the results for each site is no larger than 15 ( $\triangle$ AIC  $\leq$  15).

Criterion (3) is based on the discussion in Section 6.3. The result for sample MP01 is considered to be a record of a transitional geomagnetic field because the corresponding VGP locates at 18.7°N. However, we intend to include this record. Transitional data are usually excluded from discussions about long-term variations in the geomagnetic dipole moments. We think such omissions may cause some artefact in statistical analyses since volcanic data are random readings of the ancient geomagnetic field.



Figure 16. Example of the results with the curved NRM–TRM1\* diagram passing the quantitative selection criteria. Since the Zijderveld diagram suggests a single primary component, the curvature would not be caused by secondary magnetization. This palaeointensity may be a biased estimate (see the text).



Figure 17. Distribution of the  $\triangle$ AICs for the NRM–TRM1\* diagrams passing the quantitative selection criteria (195 specimens).

The present data set will help in studies of the time-averaged field (TAF) and palaeosecular variations (PSV). Most of the analyses (e.g. Gubbins & Kelly 1993; Johnson & Constable 1995, 1997; Kelly & Gubbins 1997; Hatakeyama & Kono 2002) only use palaeodirectional data because of the small number of existing absolute palaeointensity data (Hatakeyama & Kono 2002). Only Kono *et al.* (2000) incorporated absolute palaeointensities.

#### 7.2 Comparison with the Thellier data set

The LTD-DHT Shaw data set obtained in Section 7.1 can be compared with an available Thellier data set having the similar quality. From the latest palaeointensity database (Perrin & Schnepp 2004), Thellier data are selected using the following criteria:

(1) Ages range between 0 and 5 Ma.

(2) Palaeointensities are obtained by the Thellier method with a pTRM check (T+).

(3) The average palaeointensity for each cooling unit is calculated from no fewer than three individual determinations ( $N \ge 3$ ).

(4) The standard deviation of each average is within 20 per cent ( $\sigma \leq 20$  per cent).

Note that we do not limit the palaeomagnetic polarities, similarly to the LTD-DHT Shaw data set. Except for this point, these criteria are almost the same as those used in the previous studies with palaeointensity databases (e.g. Juarez & Tauxe 2000; Selkin & Tauxe 2000; Heller *et al.* 2002; Biggin & Thomas 2003b). Criterion (4) seems to be reasonable because Valet (2003) reviewed numerous palaeointensity results reported from the Kilauea, Hawaii, 1960 lava, and concluded that the present palaeointensity techniques could not determine the field with a precision of better than 20 per cent. The total number of selected Thellier data is 458, about half of which comprise data from the Hawaiian Islands.

The selected LTD-DHT Shaw and the Thellier data are presented in Fig. 19 with their ages. This figure indicates that there is no systematic bias in age distributions between the LTD-DHT Shaw and the Thellier data set prior to ~0.9 Ma. Most Thellier data belong to the Brunhes chron, but their VADMs do not differ significantly from those of older ages. Average VADMs are calculated for each data set:  $(3.64 \pm 2.10) \times 10^{22}$  A m<sup>2</sup> for the LTD-DHT Shaw data (N = 24) and  $(7.46 \pm 3.10) \times 10^{22}$  A m<sup>2</sup> for the Thellier data (N = 458). Although the reliability of palaeointensity determination from submarine basaltic glass is still under debate (e.g. Heller *et al.* 2002; Smirnov & Tarduno 2003), their contributions are too small to affect the present Thellier data set: if the submarine basaltic glass data are excluded, the average is  $(7.49 \pm 3.15) \times 10^{22}$  A m<sup>2</sup> (N = 434). Histograms of both data set are illustrated in Fig. 20. The average of the LTD-DHT Shaw data set is nearly half



Figure 18. Results of the LTD-Thellier (A, D, G and J), Thellier (B, E, H and K) and LTD-DHT Shaw (C, F, I and L) experiments for the sister specimens. The suffix 'L' in the specimen name indicates the result of a Thellier experiment with LTD treatment. Zijderveld diagrams are also shown as insets, where closed and open symbols indicate projections onto horizontal and vertical planes, respectively (squares are NRM before LTD).

of the mean of the Thellier data set as well as the present dipole moment.

The large discrepancy between the two data sets is probably due to the different methods of palaeointensity determination. This is because the mean VGP positions calculated from the two data set almost coincide with each other (Fig. 21), suggesting that the palaeodirections are of equivalent quality. In the calculation, the Thellier data set is split into two data sets—Hawaiian and non-Hawaiian data—since 64 per cent of the Hawaiian data (N = 148) are inclination only. Ninety-eight per cent of the non-Hawaiian data have both inclination and declination. For the LTD-DHT Shaw data set, the mean locates at 83.2°N, 353.4°E with  $\alpha_{31} = 5.9^{\circ}$  and  $\alpha_{32} =$ 8.4° ( $\alpha_{31}$  and  $\alpha_{32}$  are 95 per cent confidence limits along minor and major axes). Regarding the Thellier data set, the Hawaiian mean is expressed as a great circle with variable declinations (*D*). We calculated the mean inclination following McFadden & Reid (1982) and it was converted to VGP for 10° intervals of declination. The location of the non-Hawaiian mean is 83.9°N, 46.2°E with  $\alpha_{31} = 3.0^{\circ}$  and



Figure 18. (Continued.)

Table 4. Experimental results with the LTD-Thellier method.

Sample ID	NRM <sub>0</sub>	PTRM	$T_1 - T_2$	N	r	q	f	Slope	$F_{\rm L}$	F (TT)	PTRM tail
									$(\mu I)$	$(\mu 1)$	
MP05-05-3L	313	20-600	400-515	6	0.993	3.47	0.261	$1.72\pm0.10$	25.0	43.0	+
			500-580	6	0.998	14.5	0.596	$0.821 \pm 0.027$	25.0	20.5	+
MP07-07-3L	333	20-600	350-515	7	0.996	7.81	0.395	$2.39\pm0.10$	25.0	59.8	+
			515-580	5	0.998	10.7	0.547	$0.803\pm0.030$	25.0	20.1	+
HH09-07-4L	353	20-600	250-530	11	0.993	10.5	0.484	$3.36\pm0.14$	25.0	84.0	+
			530-580	4	0.994	3.76	0.453	$0.732\pm0.057$	25.0	18.3	_
PU06-04-4L	567	20-600	250-545	12	0.969	5.46	0.474	$6.45\pm0.50$	25.0	161	+
			545-600	4	0.993	4.45	0.607	$1.75\pm0.15$	25.0	43.7	+

NRM<sub>0</sub>, initial NRM intensity after the first LTD treatment.

Table 5. Statistical results of the palaeodirections and LTD-DHT Shaw palaeointensities.

Site	K–Ar age	Nd	Dec.	Inc.	α95	P <sub>Lat</sub>	PLong	$N_{\rm F}$	F	VDM	VADM	$\Delta AIC_{min}$
	(Ma)		(°)	(°)	(°)	(°)	(°)		(µT)	$(10^{22} \mathrm{Am^{2}})$	$(10^{22} \mathrm{Am^{2}})$	
Dykes and single lavas												
MP01		5	-80.4	-79.7	4.4	18.7	48.6	4	$4.17\pm0.32$	$0.566\pm0.043$	$0.971\pm0.075$	-2.0
(TA13)	$3.11\pm0.04$	9	158.6	37.3	6.3	-69.3	-76.6	1	10.2	2.25	2.37	21.3
(RT03)	$2.65\pm0.03$	6	1.3	-26.4	4.6	86.8	-127.8	2	$16.1\pm1.7$	$3.85\pm0.41$	$3.73\pm0.39$	5.0
(RA01)	$2.45\pm0.05$	4	6.0	-24.7	3.2	83.0	-94.1	1	12.6	3.04	2.92	6.3
PU04	$0.92\pm0.03$	6	20.3	-62.3	4.1	58.9	1.4	5	$22.4\pm0.8$	$3.74\pm0.14$	$5.15\pm0.19$	-0.5
PU05	$1.03\pm0.02$	7	19.9	-33.4	6.1	71.1	-54.7	5	$15.1\pm1.8$	$3.44\pm0.41$	$3.47\pm0.41$	4.2
TR02		6	-8.0	-23.8	5.1	80.6	154.6	4	$9.21\pm0.93$	$2.24\pm0.23$	$2.11\pm0.21$	-1.0
(TH02)	$0.72\pm0.11$	4	12.5	-29.4	4.7	77.9	-66.3	2	$27.7\pm2.4$	$6.51\pm0.57$	$6.38\pm0.56$	-0.4
TH03	—	4	4.7	-18.3	7.7	80.7	-119.6	3	$4.71\pm0.77$	$1.18\pm0.19$	$1.08\pm0.18$	1.0
(TH04)	$0.51\pm0.10$	4	7.4	-18.6	3.7	79.1	-106.9	1	9.24	2.30	2.12	25.5
Lava sequences												
(MP13)	$4.61\pm0.05$	5	-3.8	-20.2	5.3	82.9	175.5	2	$25.3\pm1.8$	$6.26\pm0.46$	$5.89\pm0.43$	10.1
(MP11)		5	2.4	-24.5	3.6	85.7	-118.5	1	24.8	6.00	5.78	16.7
(MP10)		5	0.3	-29.4	7.9	89.2	-129.9	1	19.0	4.45	4.42	7.4
(MP07)		5	-4.8	-25.3	7.7	84.4	151.1	2	$33.0\pm2.8$	$7.95\pm0.68$	$7.69\pm0.66$	34.0
(MP06)	—	5	-2.0	-27.6	6.5	87.4	161.2	2	$35.1\pm3.5$	$8.34\pm0.84$	$8.18\pm0.82$	42.6
(MP05)		5	-1.0	-25.6	2.3	86.9	-169.8	2	$31.9\pm2.1$	$7.67\pm0.51$	$7.43\pm0.49$	16.8
(MP04)	—	5	-4.7	-28.0	2.5	85.2	136.1	1	27.2	6.45	6.34	-0.6
(MP03)	—	5	0.0	-25.3	2.4	86.9	-153.0	1	32.2	7.76	7.50	18.9
MP02	$4.52\pm0.05$	5	3.3	-25.0	3.7	85.4	-107.9	3	$21.9\pm2.0$	$5.30\pm0.49$	$5.11\pm0.47$	-1.7
(BR07)	$3.67\pm0.05$	7	-176.9	24.6	4.2	-85.3	67.6	3	$23.4\pm12.3$	$5.65 \pm 2.97$	$5.44 \pm 2.85$	6.3
BR04	$3.75\pm0.05$	7	-160.4	29.6	4.2	-71.2	118.9	4	$26.5\pm3.3$	$6.22\pm0.77$	$6.18\pm0.77$	-1.9
BR15	$3.43\pm0.06$	7	-159.2	42.2	2.8	-69.0	143.9	6	$14.5 \pm 1.5$	$3.06\pm0.32$	$3.37\pm0.35$	-0.9
(BR14)		5	-160.2	37.6	3.1	-70.7	135.1	1	20.1	4.43	4.69	0.9
BR18	$3.51\pm0.05$	8	15.0	-45.8	3.2	72.4	-21.5	4	$17.4 \pm 1.1$	$3.54 \pm 0.23$	$4.05\pm0.27$	-0.1
(TA07)	$3.24\pm0.05$	5	-67.4	70.3	5.3	-1.1	176.0	1	4.46	0.670	1.04	9.3
TA11	$2.57\pm0.13$	7	173.4	22.6	12.4	-81.9	-25.1	3	$23.1\pm0.8$	$5.65 \pm 0.18$	$5.37\pm0.18$	-1.8
TA08	$3.14\pm0.06$	7	179.1	17.8	7.5	-82.4	21.7	5	$23.8\pm3.9$	$5.96 \pm 0.97$	$5.54\pm0.90$	7.4
(TA19)		5	-12.9	-54.3	9.2	68.5	58.4	1	8.96	1.65	2.08	1.5
(TA17)	$2.99 \pm 0.04$	7	-16.8	-59.0	6.0	62.6	57.4	2	$5.68 \pm 1.17$	$0.986 \pm 0.203$	$1.32 \pm 0.27$	-0.7
TA16	$2.97 \pm 0.04$	5	-5.9	-60.9	7.7	64.2	38.7	4	$3.02 \pm 0.40$	$0.512 \pm 0.068$	$0.701 \pm 0.093$	-2.0
(TA15)	$2.90 \pm 0.05$	7	-23.0	-49.2	2.0	65.1	81.8	5	$7.36 \pm 0.71$	$1.44 \pm 0.14$	$1.71 \pm 0.17$	18.5
(RT05)		6	2.7	51.7	3.0	40.7	-148.4	1	5.20	0.989	1.21	14.4
(RT10)	$2.76 \pm 0.03$	7	-41.4	-28.3	9.3	50.2	115.2	3	$4.23 \pm 1.39$	$1.00 \pm 0.33$	$0.981 \pm 0.322$	-1.3
RT12m	$2.61 \pm 0.03$	7	7.3	-39.2	2.0	81.3	-22.3	6	$8.67 \pm 1.03$	$1.88 \pm 0.22$	$2.01 \pm 0.24$	-1.9
RT18m	$2.67 \pm 0.03$	6	14.3	-24.7	4.9	75.6	-75.2	4	$9.03 \pm 1.08$	$2.18 \pm 0.26$	$2.09 \pm 0.25$	5.5
(HH01)	$2.72 \pm 0.03$	7	3.1	-22.8	1.8	84.2	-119.0	1	38.4	9.39	8.91	28.8
HH11m	$3.09 \pm 0.04$	6	7.0	-26.8	4.4	82.7	-81.3	4	$15.1 \pm 1.5$	$3.60 \pm 0.36$	$3.50 \pm 0.35$	9.7
HH09	_	7	22.3	-31.1	3.4	68.7	-57.8	5	$17.8 \pm 1.0$	$4.12 \pm 0.22$	$4.12 \pm 0.22$	0.0
HH16		7	9.9	-34.6	2.1	80.3	-45.8	5	$33.9 \pm 3.4$	$7.65 \pm 0.76$	$7.86 \pm 0.79$	4.1
HH20	$2.83 \pm 0.09$	7	1.3	-40.8	1.7	83.3	18.7	4	$38.4 \pm 2.1$	$8.21 \pm 0.46$	$8.91 \pm 0.49$	-1.2
MR01	$1.58 \pm 0.04$	7	170.4	31.0	2.4	-80.8	-56.0	5	$15.0 \pm 1.0$	$3.49 \pm 0.23$	$3.45 \pm 0.22$	-1.8
(MR02)		5	172.6	29.5	3.9	-82.6	-46.6	1	7.55	1.77	1.74	20.4
(MR04)		5	172.3	37.9	0.9	-81.9	-88.3	1	11.4	2.50	2.62	11.4
MR06	$1.62 \pm 0.08$	7	173.5	30.5	4.8	-83.7	-50.0	5	$8.72 \pm 0.64$	$2.03 \pm 0.15$	$2.00 \pm 0.15$	-1.9
(MR09)	—	5	163.6	34.1	4.6	-74.4	-66.4	1	26.6	6.04	6.11	-1.2
(MR12)	—	5	174.9	29.3	3.3	-84.7	-39.6	1	20.6	4.84	4.74	-0.3
(MR14)		5	174.1	25.4	4.8	-82.9	-24.2	1	27.6	6.65	6.34	1.3
MR16	$1.51 \pm 0.04$	7	174.1	32.8	3.0	-84.4	-63.2	3	$9.52 \pm 1.03$	$2.18 \pm 0.24$	$2.19 \pm 0.24$	1.0
(MR22)		5	168.0	56.4	4.4	-67.9	-123.6	1	13.1	2.35	3.01	0.5
MR23	$1.55 \pm 0.06$	7	181.8	61.4	6.0	-64.9	-153.0	6	$13.0 \pm 2.1$	$2.20 \pm 0.36$	$3.00 \pm 0.49$	-2.0
MR32	$1.50 \pm 0.04$	7	185.7	68.0	3.6	-56.2	-156.2	7	$13.3 \pm 2.4$	$2.05 \pm 0.36$	$3.05 \pm 0.54$	-1.5
PU01	$1.12\pm0.02$	7	160.8	33.1	4.6	-71.8	-63.9	4	$9.50\pm0.87$	$2.17\pm0.20$	$2.18\pm0.20$	-1.5

Site, site ID;  $N_d$ , number of the specimens used for the calculation of palaeodirection; Dec., Inc.,  $\alpha_{95}$ , palaeodirection and its 95 per cent confidence circle;  $P_{Lat}$ ,  $P_{Long}$ , latitude and longitude of the virtual geomagnetic pole;  $N_F$ , number of the specimens used for the calculation of mean palaeointensity; F, VDM, VADM, mean palaeointensity, virtual dipole moment and virtual axial dipole moment with their standard deviations;  $\Delta AIC_{min}$ , minimum  $\Delta AIC$  values for the individual sites. Note that the mean palaeointensity is calculated without the outliers (multispecimen test) for the site ID with suffix of 'm'. K–Ar ages and palaeodirections are referred from Uto *et al.* (submitted) and Yamamoto *et al.* (2002).



**Figure 19.** VADM variations for the period of the last 5 Myr. Open symbols indicate the selected Thellier data (N = 458) while closed ones correspond to the LTD-DHT Shaw palaeointensities (N = 21; note that VADMs of the sites MP01, TR02 and TH03 are not indicated because of undetermined K–Ar ages). The selections are mainly based on the criteria of  $N \ge 3$  and  $\sigma \le 20$  per cent (see text). About half of the Thellier data are Hawaiian data (N = 232, triangles). The geomagnetic polarity timescale (radiometric timescale) is from Singer *et al.* (2002) and Uto *et al.* (submitted).

 $\alpha_{32} = 4.2^{\circ}$ . Note that the means except for the Hawaiian data are evaluated by the Bingham statistics because their elongation parameters ( $\alpha_{32}/\alpha_{31}$ ; Tanaka 1999) are large (1.41 and 1.39).

We consider that the average calculated from the present LTD-DHT Shaw data set is more appropriate for the mean VADM of the last 5 Myr. As mentioned in Section 1, the Thellier method occasionally fails in accurate determinations of palaeointensity from historical lavas. Fig. 22 (A) summarizes the intensities reported from historical lavas (Tanaka & Kono 1991; Tanaka *et al.* 1995a; Hill & Shaw 2000; Calvo *et al.* 2002; Böhnel *et al.* 2003; Yamamoto *et al.* 2003; Mochizuki *et al.* 2004; Oishi *et al.* 2005). Almost all the reported Thellier palaeointensities are overestimates, which are as high as 200 per cent of the expected value. On the other hand, LTD-DHT Shaw palaeointensities from the same lavas (Yamamoto *et al.* 2003; Mochizuki *et al.* 2004; Oishi *et al.* 2005) are clustered around the expected value except for some outliers (Fig. 22B). These observations can explain the large discrepancy in the 0–5 Ma mean VADMs between the LTD-DHT Shaw and the Thellier data set.

# 7.3 Overestimated palaeointensities in the Hawaiian Thellier data set

The overestimated palaeointensities might be especially accumulated in the Hawaiian data set. If average VADMs are calculated separately for the Hawaiian and non-Hawaiian Thellier data sets, they give  $(8.10 \pm 2.62) \times 10^{22}$  A m<sup>2</sup> (N = 232) and (6.80 ± 3.41)  $\times$  10<sup>22</sup> A m<sup>2</sup> (N = 226), respectively (Fig. 20). The F-test and ttest for these values gave an F value of 1.69 and a t value of 4.60, both of which correspond to probabilities of <0.0001. This situation is almost unchanged even if the submarine basaltic glass data are excluded: average VADMs are calculated to be (8.21  $\pm$  2.71)  $\times$  $10^{22}$  A m<sup>2</sup> (N = 211, Hawaiian data) and (6.80 ± 3.39) ×  $10^{22}$  A m<sup>2</sup> (N = 223, non-Hawaiian data). The Hawaiian and non-Hawaiian data set are statistically distinguishable from each other. As discussed in the previous subsection, the mean VGP positions from the two data set do not significantly differ from each other (Fig. 21). Thus, the difference could be solely attributed to quality of the reported palaeointensities.

The high palaeointensities in the Hawaiian data set possibly originate from ancient lavas with NRMs of non-TRM origin. For example, the data set includes 10 results from 2.1-3.9 Ma lavas in Oahu, Hawaii (Laj et al. 2000). One of their Arai diagrams (KO26-146B; Fig. 5 of Laj et al. 2000) appears to be two-segmented. Seventythree results came from the Hawaiian Scientific Drilling Program (HSDP) cores studied by Laj & Kissel (1999). Thermomagnetic analyses indicated the presence of low-Ti titanomagnetites in  $\sim 85$ per cent of their samples. Recently, Kontny et al. (2003) have extensively studied the thermomagnetic properties of samples from the subaerial part of the HSDP2 cores and classified the properties into three types. Two of them resulted in Curie temperatures of 480-600 °C. They reported that the ore mineral textures of these two types were characterized by titanomagnetites with ilmenite lamellae. These features resemble those of the Kilauea 1960 lava which yields a number of anomalously high palaeointensities with the Thellier method (Yamamoto et al. 2003). They suggested that its main cause was NRM of non-TRM origin.

The possibility of biased palaeointensities in the Hawaiian data set is also supported from recently reported Thellier results from submarine basaltic glass of HSDP2 cores (Tauxe & Love 2003). Although the reliability of palaeointensity determination on submarine basaltic glass is still under debate, as stated before, Tauxe & Love (2003) carefully examined the rock magnetic properties of their



**Figure 20.** Histograms of the VADMs for (A) the Thellier and (B) the LTD-DHT Shaw data set. Average VADMs are calculated to be  $(7.46 \pm 3.10) \times 10^{22}$  A m<sup>2</sup> (N = 458, Thellier) and  $(3.64 \pm 2.10) \times 10^{22}$  A m<sup>2</sup> (N = 24, LTD-DHT Shaw) for each data set. If the Thellier data set is split into two data sets—Hawaiian and non-Hawaiian—they result in average VADMs of  $(8.10 \pm 2.62) \times 10^{22}$  A m<sup>2</sup> (N = 232) and  $(6.80 \pm 3.41) \times 10^{22}$  A m<sup>2</sup> (N = 226), respectively. They are statistically distinguishable by both the *t*-test and the *F*-test at >99.9999 per cent confidence (see text).



**Figure 21.** Mean VGP positions of the LTD-DHT Shaw and Thellier data set. The former mean locates at  $83.2^{\circ}$ N,  $353.4^{\circ}$ E with  $\alpha_{31} = 5.9^{\circ}$  and  $\alpha_{32} = 8.4^{\circ}$  (closed triangle). As for the latter, the data set is split into Hawaiian and non-Hawaiian data. The position of the Hawaiian data is expressed as a great circle with variable declination (*D*) indicated by closed circles. The mean of the non-Hawaiian data locates at  $83.9^{\circ}$ N,  $46.2^{\circ}$ E with  $\alpha_{31} = 3.0^{\circ}$  and  $\alpha_{32} = 4.2^{\circ}$  (closed square).

samples and showed their robustness to Thellier palaeointensity determinations. As a result, they obtained Thellier palaeointensities spanning 440-550 kyr from 34 cooling units. If these data are subjected to the same statistical criteria as described in the previous subsection (N > 3 and  $\sigma < 20$  per cent), 21 site means can be selected (note that these data are already included in the Hawaiian Thellier data set). They give an average VADM of (7.02  $\pm$  0.87)  $\times$  10<sup>22</sup> A m<sup>2</sup>. This is almost the same as the average VADM of the non-Hawaiian data set [( $6.80 \pm 3.41$ ) ×  $10^{22}$  A m<sup>2</sup>, N = 226]. Although the time coverage of the data of Tauxe & Love (2003) is very short, the duration of  $\sim 100$  kyr is thought to be sufficient to represent the palaeosecular variation (Tanaka & Kobayashi 2003). Also, in the Brunhes chron, a VADM of ~100 kyr scale average does not appear to show significant variations in relative palaeointensities from sediments (e.g. Guyodo & Valet 1999; Yamazaki 2002) and deep-tow magnetic anomalies (e.g. Gee et al. 2000). This feature is unchanged prior to the Matuyama chron (e.g. Kok & Tauxe 1999; Pouliquen et al. 2001; Yamazaki & Oda 2002). Thus, the two average VADMs seem to be comparable. Submarine basaltic glass is generally believed not to suffer from deuteric oxidation. Its rock magnetic properties are thought to be different from those of subaerial lavas such as the Kilauea 1960 lava. The coincidence between the two average VADMs suggests a relatively smaller probability of biased palaeointensities in the non-Hawaiian data set. However, it is emphasized that the non-Hawaiian data set still gives an average VADM twice as large as that obtained with the LTD-DHT Shaw data set.

#### 8 CONCLUSIONS

We have performed various rock magnetic measurements and palaeointensity determinations on 0.5–4.6 Ma volcanic rocks collected from the Society Islands, French Polynesia.

(1) Based on the thermomagnetic analyses, low-temperature magnetometry and hysteresis measurements, the main remanence carriers are identified to be titanomagnetites with different Ti contents. Some samples additionally contain a minor amount of Ti-rich titanomagnetites. They are considered to be an admixture of SD (and/or PSD) and MD, and the MD content is not too large. Reflected-light microscopy suggests that many of the present samples contain intermediately high-temperature-oxidized titanomagnetite grains (C3–C4). They are possible candidates for giving anomalously high palaeointensities in Thellier experiments but not in LTD-DHT Shaw experiments.

(2) LTD-DHT Shaw experiments gave 195 out of 361 successful palaeointensity determinations with the quantitative selection criteria. They are independent of the hysteresis properties and not thought to be systematically influenced by the ARM correction.

(3) Thellier experiments were conducted on 40 selected specimens with good thermal stability. Their sister specimens had already given successful results in the LTD-DHT Shaw experiments. The selection criteria admit 18 palaeointensities, but they contain a number of anomalous results. Many of them are characterized by two-segmented Arai diagrams. If we add a criterion of  $f \ge 0.50$ , 13 results survive and these palaeointensities seem to be improved.





Figure 22. Compilation of the reported palaeointensities from historical lavas. The Thellier and LTD-DHT Shaw data (Tanaka & Kono 1991; Tanaka *et al.* 1995a; Hill & Shaw 2000; Calvo *et al.* 2002; Böhnel *et al.* 2003; Yamamoto *et al.* 2003; Mochizuki *et al.* 2004; Oishi *et al.* 2005) are separately illustrated in (A) and (B), respectively. The abscissa indicates normalized palaeointensities divided by the expected field intensity while the ordinate shows each reference. Note that the microwave Thellier palaeointensities of Hill & Shaw (2000) are adopted from the first slopes when corresponding specimens yielded two-segmented Arai diagrams. The palaeointensities of Böhnel *et al.* (2003) are compared with the contemporaneous global mean of Yang *et al.* (2000).

Discrepancies between the Thellier and the LTD-DHT Shaw palaeointensities are up to about 40 per cent for the sister specimens, which is similar to the results from the historical lavas by Yamamoto *et al.* (2003), Mochizuki *et al.* (2004) and Oishi *et al.* (2005).

(4) The reliability of the successful LTD-DHT Shaw results was further examined from several aspects. Possible low-temperature oxidation and inapplicability of the ARM corrections were suggested for 40 specimens. These may be sources of biased palaeointensities. Some part of the successful results also showed upward convexity in the NRM–TRM1\* diagrams, which may have equivalent qualities to Thellier palaeointensity results with concave Arai diagrams. According to the growing consensus on analyses of Thellier results, it seems better not to use such LTD-DHT Shaw palaeointensities. This convexity could be evaluated by  $\Delta$ AIC. Although it is difficult to define an exact threshold  $\Delta AIC$ , we temporarily take a threshold value of 15 in this study. There are 49 results with  $\Delta AIC > 15$  among the present successful results.

(5) We can pick up 24 reliable site-mean palaeointensities from the newly obtained LTD-DHT Shaw data set. They give the average VADM of  $(3.64 \pm 2.10) \times 10^{22}$  A m<sup>2</sup> for the last 5 Myr. This is nearly half of the mean of the 0–5 Ma Thellier data selected from the latest palaeointensity database [(7.46 ± 3.10) × 10<sup>22</sup> A m<sup>2</sup>, N = 458]. The large discrepancy between the two averages originates from the difference in the palaeointensity techniques.

(6) We consider that the average VADM by the present LTD-DHT Shaw data set is more appropriate for the mean of the last 5 Myr. This is because the Thellier method occasionally gives overestimated palaeointensities as high as 200 per cent of the true value while the LTD-DHT Shaw method does not. In particular, overestimated palaeointensities might be accumulated in the Hawaiian data set. Many results in this data set might suffer from NRMs of non-TRM origin. The newly determined LTD-DHT Shaw palaeointensities indicate that the present dipole moment ( $\sim 8 \times 10^{22}$  A m<sup>2</sup>) is about twice the time average for the last 5 Myr. The characteristics of the present field may not be typical of the geomagnetic field. We have to be careful when extending the characteristics of the present-day field to the ancient field.

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